#### 20<sup>th</sup> NATIONAL CERTIFICATION EXAMINATION FOR ENERGY MANAGERS & ENERGY AUDITORS – September, 2019

PAPER – 3: ENERGY EFFICIENCY IN ELECTRICAL UTILITIES

#### Section – I: OBJECTIVE TYPE

Marks: 50 x 1 = 50

- i) Answer all **50** questions
- ii) Each question carries **one** mark
- iii) Please hatch the appropriate oval in the OMR answer sheet with HB pencil only, as per instructions

| 1. | In a pumping system, if the temperature of the liquid handled increases then   |  |  |  |  |  |
|----|--|--|--|--|--|--|
|    | a) NPSHa increases   |  |  |  |  |  |
|    | b) NPSHa decreases   |  |  |  |  |  |
|    | d) NPSHa and NPSHr are independent of temperature  |  |  |  |  |  |
| 2. | Which of the following component has maximum effect on cooling tower performance?  |  |  |  |  |  |
|    | a) <u>Fill media</u> b) drift c) louvers d) casing   |  |  |  |  |  |
| 3. | In a vapour compression refrigeration system, the quantum of energy transferred condenser is more than the energy transferred at       |  |  |  |  |  |
|    | a) Compressor  |  |  |  |  |  |
|    | b) Expansion Valve<br>c) Evaporator  |  |  |  |  |  |
|    | d) <u>All of the above</u>   |  |  |  |  |  |
| 4. | Demand side Management helps   |  |  |  |  |  |
|    | a) to reduce the energy losses b) to reduce system peak demand c) to promote energy efficiency among users. d) <u>All of the above</u> |  |  |  |  |  |
| 5. | Which one of the following is true to estimate the range of cooling tower?   |  |  |  |  |  |
|    | a) Range = Cooling water inlet temperature – Wet bulb temperature  |  |  |  |  |  |
|    | b) Range = Cooling water outlet temperature – Wet bulb temperature   |  |  |  |  |  |
|    | d) <u>None of the above</u>  |  |  |  |  |  |
| 6. | Modest flow variation between 80% to 100%, in a centrifugal fan is achieved more efficiently with                                      |  |  |  |  |  |
|    | a) Inlet damper  |  |  |  |  |  |
|    | b) Outlet damper   |  |  |  |  |  |
|    | d) Impeller Change   |  |  |  |  |  |
| 7. | is used as refrigerant both in vapour compression and vapour absorption systems  |  |  |  |  |  |
|    | a) Lithium Bromide b) Water c) HFC 134A d) <u>Ammonia</u>  |  |  |  |  |  |

| 8.  | In electrical distribution system, commercial loss covers discrepancies due to  |
|-----|---|
|     | a) Meter Reading b) Metering c) Collection Efficiency d) All of the above   |
| 9.  | Which of the following parameters is not required for evaluating volumetric efficiency of                                   |
|     | reciprocating air compressor?   |
| 10  | a) <u>rower input</u> b) FAD c) Cylinder Stroke d) Cylinder bore  |
| 10. |   |
|     | a) Variable Frequency drive b) Soft starter   |
|     | c) Hydraulic coupling   |
| 11  | d) Eddy current drives  |
|     | a) Higher slip  |
|     | b) Higher starting torque<br>c) Lower No load current   |
|     | d) All the above  |
| 12. | For a given air requirement, providing higher volume air receiver will  |
|     | a) Increase energy consumption  |
|     | c) Reduce energy consumption<br>c) Reduce Unload Power  |
|     | d) <u>Reduce Pressure fluctuations</u>  |
| 13. | Harmonics generation will be more in  |
|     | a. Inverter drives b. LED Lamps c. Transformers d. Resistance heaters   |
| 14. | Thermal Power Plant efficiency is low due to  |
|     | a) Higher steam Pressure  |
|     | <ul> <li>c) Low GCV coal</li> </ul>   |
|     | d) <u>Higher Heat loss in condenser</u>   |
| 15. | Among the following, has highest design efficiency.   |
|     | a) High tension motors  |
|     | c) Alternators  |
|     | d) Electric melting furnaces  |
| 16. | The difference between wet bulb temperature and cooling water inlet temperature in a cooling tower is called                |
|     | a) Approach b) Range c) Effectiveness d) None of the above  |
| 17. | Technical loss in a distribution system can be reduced by   |
|     | a) Maintaining low HT/LT ratio  |
|     | a) Maintaining low FITE Failob) Accurate meter readingc) High voltage supply to consumersd) Improving Collection Efficiency |
| 18. | Pressure drop can be reduced in a compressed air distribution line by providing   |
|     | ································  |

|     | <ul> <li>a) After Coolers</li> <li>b) Small diameter distri</li> <li>c) High pressure air flor</li> <li>d) Large Diameter District</li> </ul>        | bution pipes<br>w<br><mark>tribution pipes.</mark> |   |   |
|-----|--|--|---|---|
| 19. | Power consumption is<br>a) Refrigeration type<br>b) Blower reactivated ty<br>c) Heat of compression<br>d) <u>Heatless purge typ</u>                  | very high for<br>/pe<br>type<br><u>e</u>           | type of compres                                       | sed air dryers.   |
| 20. | A DC excitation is used  | I to vary the speed of _                           |   |   |
|     | <ul> <li>a) Eddy Current Coupling</li> <li>b) fluid coupling</li> <li>c) variable frequency of</li> <li>d) None of the above</li> </ul>              | <mark>pling</mark><br>drive                        |   |   |
| 21. | The isothermal power actual power drawn by   | of 500 CFM air compr<br>the compressor will be     | essor is 72 kW and                                    | the efficiency is 76 %. The                               |
|     | a) 56 kW   | <u>b) 94.7 kW</u>                                  | c) 89 kW  | d) 72 kW  |
| 22. | Power factor improvem  | ent of a 75-kW compre                              | essor motor will                                      |   |
|     | a) Reduce input power<br>c) Reduce the compres   | to the motor<br>sor motor shaft power              | b) Increase<br>d) <mark>None of</mark>                | input power to the motor<br>the above                     |
| 23. | A 500-kVA transformer<br>The calculated total tra<br>the transformer?  | is designed for No loa<br>ansformer loss is 1662   | d loss of 750 watts a<br>watts. What will be          | and load loss of 5700 Watts.<br>The percentage loading of |
|     | a) 54.8 %  | b) 29 %  | c) <u>40 %</u>  | d) 25.7 %   |
| 24. | Rating of PF correction  | capacitors for Inductio                            | n Motors terminal sh                                  | ould be   |
|     | <ul> <li>a) 100 % kVAr of the in</li> <li>b) 20 % of Motor Rating</li> <li>c) 25 % of Motor rating</li> <li>d) <u>90 % of the no-load</u></li> </ul> | duction motor<br>g<br>I kVAr induction moto        | <u>or</u>   |   |
| 25. | LLF in lighting calculati  | on refers to                                       |   |   |
|     | <ul> <li>a) Light Load factor</li> <li>b) Light lumen factor</li> <li>c) Light Lux factor</li> <li>d) Light loss factor</li> </ul>                   |  |   |   |
| 26. | A medium voltage end cascade efficiency of 82  | consumer receives 83<br>2%. The million units ge   | million units with a tree merated will be             | ransmission and distribution                              |
|     | a) <u>101.2</u>  | b) 68.1  | c) 83   | d) None of the above                                      |
| 27. | A 1000 kW Gas engine<br>825 kW. If the GCV<br>m³/hr  | e is designed for 38 %<br>/ of gas is 8700 ki      | b efficiency. The ope cal/m <sup>3</sup> , the hourly | rating load of the engine is gas consumption will be      |
|     |  | h) 260 13  | c)188 89  | d) 272 74   |

| 28. | In an electrical power system, transmission efficiency increases as  |
|-----|--|
|     | a) both voltage and power factor increases   |
|     | b) both voltage and power factor decrease  |
|     | c) voltage increases but power factor decreases  |
|     | d) Voltage decreases but power factor increases.   |
| 29. | Which of the following is expressed in terms of percentage?  |
|     | a) Absolute humidity   |
|     | b) <u>Relative humidity</u>  |
|     | c) Specific Gravity  |
|     |  |
| 30. | Which among the following is one of the parameters used to classify fans, blowers & Compressors?   |
|     | a) Volume flow rate  |
|     | b) Mass flow rate  |
|     | c) <u>Specific ratio</u>   |
|     | d) None of the above   |
| 31. | What is the function of drift eliminators in cooling towers?   |
|     | a) maximize water and air contact  |
|     | b) capture water droplets escaping with air stream   |
|     | c) enables entry of air to the cooling tower   |
|     | a) eliminates uneven distribution of water into the cooling tower  |
| 32. | Which of the following statements is not true regarding centrifugal pumps?   |
|     | a) Flow is zero at shut off head   |
|     | b) Maximum efficiency will be at design rated flow of the pump   |
|     | c) Head decreases with increase in flow  |
|     | a) Power increases with throttling   |
| 33. | Which of the following is not true with respect to Color Rendering Index (CRI)?  |
|     | a) The CRI is expressed in a relative scale ranging from 0 -100.   |
|     | b) CRI indicates, how perceived colors match with actual colors.   |
|     | <ul> <li>c) LED lamps are having comparatively higher CRI than incandescent Lamps.</li> <li>d) The higher the color rendering index, the lass color shift or distortion occurs.</li> </ul> |
| 0.4 | (a) The higher the color rendering index, the less color shift of distortion occurs  |
| 34. | curve.   |
|     | a) Inlet guide vane  |
|     | b) speed change with variable frequency drive  |
|     | c) speed change with hydraulic coupling  |
|     | d) <u>discharge damper</u>   |
| 35. | The primary purpose of inter-cooling in a multistage compressor is to  |
|     | a) remove the moisture in the air  |
|     | b) reduce the work of compression  |
|     | c) separate moisture and oil vapour  |

|     | d) none of the a   | above  |  |                               |  |
|-----|--|--|--|-------------------------------|--|
| 36. | Illuminance of a su  | rface is expressed in  | I  |                               |  |
|     | a) radians   | b) <u>lux</u>  | c) lumens  | d) LPD                        |  |
| 37. | A pump discharge has to be reduced from 120 m <sup>3</sup> /hr to 110 m <sup>3</sup> /hr by trimming the impeller. What should be the percentage reduction in impeller size? |  |  |                               |  |
|     | a)10.52 %  | b) <u>8.34%</u>  | c) 9.7 1%  | d)17.1%                       |  |
| 38. | Which of the follow<br>a) Open cycle<br>b) Diesel Engir<br>c) <u>Combined (</u><br>d) Conventiona  | ring power plants has<br>Gas Turbine<br>ne<br><mark>cycle gas turbine</mark><br>al coal plants                             | the highest efficiency?  |                               |  |
| 39. | COP of a single eff<br>of  | ect absorption refrig  | eration system is likely t                                       | o be in the range             |  |
|     | a) <u>0.6 to 0.7</u>   | b) 1to 1.2   | c) 1.5 to 2  | d) 3.0 to 4.0                 |  |
| 40. | If 30240 kcal of he be nearly equal to   | eat is removed from a  | a room every hour then t   | he refrigeration tonnage will |  |
|     | a) 30.24TR   | b) 3.024TR   | c) 1TR   | d) <u><b>10 TR</b></u>        |  |
| 41. | <ul> <li>HVDS (High Voltage)</li> <li>a) <u>Reduce tec</u></li> <li>b) Reduce com</li> <li>c) Reduce cap</li> <li>d) Reduce ene</li> </ul>                                   | ge Distribution Syster<br>hnical loss in distril<br>imercial loss in distril<br>ital investment<br>rgy bill for the end co | m) is preferred to<br>bution system<br>oution system             |                               |  |
| 42. | When evaporator t  | emperature is reduce   | ed,  |                               |  |
|     | <ul> <li>a) refrigeration</li> <li>b) refrigeratio</li> <li>c) specific pow</li> <li>d) condenser less</li> </ul>  | capacity increases<br>n capacity decrease<br>er consumption rema<br>pad increases  | es<br>ains same  |                               |  |
| 43. | A 4 pole 50 Hz induction motor is running at 1470 rpm. What is the slip value?   |  |  |                               |  |
|     | a) 0.2   | b) <u>0.02</u>   | c) 0.04  | d) 0.4                        |  |
| 44. | The basic function   | The basic function of an air dryer in an air compressor is to  |  |                               |  |
|     | <ul> <li>a) Prevent dus</li> <li>b) Remove mo</li> <li>c) Remove mo</li> <li>d) <u>Remove mo</u></li> </ul>  | t from entering the co<br>isture before the inte<br>isture in compressor<br>pisture in air supplice                        | ompressor<br>rcooler<br>suction<br><mark>ed to the plants</mark> |                               |  |
| 45. | Power factor is hig<br>a) Sodium vap<br>b) Induction lai<br>c) LED Lamps<br>d) Incandesce  | hest in the case of<br>our lamps<br>nps<br><mark>nt lamps</mark>   |  |                               |  |

| 46. | If the COP of a vapour compression system is 3.5 and the motor draws a power of 10.8 kW at 90% motor efficiency, the cooling effect of vapour compression system will be |  |                                  | s a power of 10.8 kW at<br>n will be |
|-----|--|--|----------------------------------|--------------------------------------|
|     | a) <u>34 kW</u>  | b) 42 k\                                 | N c) 2.8 kW                      | d) 3.4 kW                            |
| 47. | The blow down requi  | irement in m <sup>3</sup> /hr of a c<br> | ooling tower with evaporation    | on rate of 16 m <sup>3</sup> /hr and |
|     | a) 4   | b) 5.3                                   | c) <u>8</u>                      | d ) 48                               |
| 48. | The percentage redute to 0.95 is   | iction in distribution los<br>           | ses when tail end power fa       | ctor is raised from 0.8              |
|     | a) <u>29.4%</u>  | b)15.5%                                  | c)16.6%                          | d)24.7%                              |
| 49. | Energy performance<br>consumption to<br>a) <u>Built up area</u><br>b) Carpet area<br>c) Roof Area<br>d) Window and Wal   | index (EPI) kWh/m² /y<br>                | r is the ratio of total building | g annual energy                      |
| 50. | Which of the followin  | g is not a climate zone                  | as per ECBC classification       | ר?                                   |
|     | a) hot-dry   | b) warm-humid                            | c) <u>Cold-humid</u>             | d) cold                              |

..... End of Section – I .....

#### Section – II: SHORT DESCRIPTIVE QUESTIONS

Marks: 8 x 5 = 40

- (i) (ii) Answer all <u>**Eight**</u> questions Each question carries <u>**Five**</u> marks

| S-1 | One of the Machining centres has installed 2 No's operation and also for cleaning operation of compone operated at 7 kg/cm <sup>2</sup> (g) and are on-load for 80 % of Power of each 270 cfm compressor is, 40 kW and 15 I that cleaning air requirement is 60% of the air generated | s of 270 cfm compressors for pneumatic<br>ents after machining. The compressors are<br>the time. The load Power and the un-load<br>kW respectively. The energy audit estimated<br>ed. |  |  |  |
|-----|---|---|--|--|--|
|     | Calculate the daily energy consumption for cleaning a the compressor.   | air alone, assuming continuous operation of   |  |  |  |
|     | Ans :   |   |  |  |  |
|     | Compressor capacity<br>% Loading<br>Air Delivered by 2 compressors<br>Loading Power drawn by the compressors<br>Un-Loading power drawn by the compressors   | = 270 cfm<br>= 80 %<br>= (270 X 0.80 x 2)<br>= 432 cfm<br>= (40 + 40)<br>= 80 kW<br>= (15 + 15)   |  |  |  |
|     | Average kW drawn by the compressors   | = 30 kW<br>= [(80 x (0.8 x24))+ (30x (0.2 x 24))]/(24)<br>= 70 kW   |  |  |  |
|     | SEC of compressor   | = (70/432)<br>= 0.162 kW/cfm  |  |  |  |
|     | Cleaning air consumption at 7 Kg/cm <sup>2</sup>  | = (60 % of generation)<br>= (0.60 x 432)<br>= 259 cfm   |  |  |  |
|     | Energy requirement for Cleaning air per day   | = (259 x 0.162 x 24)<br>= <b>1007 kWh/day</b>   |  |  |  |
|     | (or) Alternate Solution   |   |  |  |  |
|     | = (Load Power )<br>= (40 x 0.8) + (1<br>= 32+3<br>= 35 KW   | x load time) + (Unload Power x Unload time)<br>5 x 0.2)   |  |  |  |
|     | Average KW drawn by the compressors $= 35 \times 2 = 35 \times 2$   | 70 KW   |  |  |  |
|     | Energy requirement for Cleaning air per day = (70 kW =<br>=1008 kW  | x 0.6) x 24<br><b>/h/day</b>  |  |  |  |
| S-2 | In a pharmaceutical industry a centrifugal pump is pu   | imping 80 m <sup>3</sup> /hr of water into a pressurized  |  |  |  |

|             | container. The container pressure is 3 kg/cm <sup>2</sup> (g). The discharge head of the pump is 5 kg/cm <sup>2</sup> (g) and water level is 5 meters below the pump central line. If the power drawn by the motor is 22 kW, find out the pump efficiency. Assume motor efficiency as 90% and the water density as 1000 kg/m <sup>3</sup> . |  |   |  |
|-------------|---|--|---|--|
| S-2-<br>Sol | Ans:  |  |   |  |
|             | SI.<br>No.  | Parameter  | Process   | Value  |
|             | 1   | Water Flow Rate (m <sup>3</sup> /hr)   | given   | 80   |
|             | 2   | Discharge Head (meters)  | given   | 50   |
|             | 3   | Suction Head (meter)   | given   | -5   |
|             | 4   | Power input to Motor (kW)  | given   | 22   |
|             | 5   | Motor Efficiency   | given   | 90%  |
|             | 6   | Power Input to Pump (kW)   | SI. 4* SI. 5  | $=22 \times 0.9 = 19.8$<br>= (80/3600) x (50 -                 |
|             |   |  | SI. 3)*9.81   | (-5) x 9.81=11.98  |
|             | 8   | Pump Efficiency  | SI. 7 / SI. 6   | 60.56%   |
|             | Inlet e<br>Outlet<br>Specif<br>Calcul   | A refrigeration system designed with 10 TR AHU is operating at 8.25 TR. The measured a parameters are given below:<br>Inlet enthalpy = 10.26 kcal/kg<br>Outlet enthalpy = 7.26 kcal/kg.<br>Specific volume of air = 0.83 m <sup>3</sup> /kg<br>Calculate the volume of air in m <sup>3</sup> /hr handled by AHU. |   |  |
|             | Ans :   |  |   |  |
|             | Cooling delivered (TR<br>= (Difference in enthalpy) x (Volume of air / sp. volume x 3024)<br>= (Hi - Ho) x V / (v x 3024)<br>= (TR x v x 3024 / (Hi - Ho))<br>= ((8.25 x 0.83 x 3024) / (10.26-7.26))<br>= <b>6903 m<sup>3</sup>/hr</b>   |  | ne of air / sp. volume x 3024)<br>26))                |  |
| S4          | A fan<br>Hz for<br>and th   | is designed for 1300 m <sup>3</sup> /hr, 50 Hz<br>6000 hours, calculate the velocity on<br>he annual energy savings.   | and drawing 3 kW. If the of air, when air is supplied | fan is operated with VFD at 37<br>through 150 mm diameter duct |
|             | Ans :   |  |   |  |
|             | Power<br>Opera<br>Flow a  | Drawn at 50 HZ<br>ting frequency<br>at 37 Hz   | = 3 k<br>= 37<br>= 130<br>= 96                        | :W<br>Hz<br>00 x (37 / 50)<br>2 m³/hr<br>0 mm                  |
|             | Area c  | of the duct  | = 15<br>= 0.0   | )177 m <sup>2</sup>  |

|    | Velocity of the air in the duct   | = [(962 / 3600)] / [(0.0177)]  |
|----|---|--|
|    | Power consumption with 37 Hz  | $= (37/50)^3 \times 3$   |
|    | Annual Energy Savings for 6000 hours ope  | ration = $1.22 \text{ kW}$<br>= $6000 \text{ x} (3 - 1.22)$  |
|    |   | = 10,680 kWh   |
| S5 | A foundry unit draws power to the tune o operation is given below:  | f 2500 kW. The demand observed during furnace  |
|    | 5 minutes : 2940 kVA<br>7 minutes : 2550 kVA<br>3 minutes : 2777 kVA  |  |
|    | If the billing meter is monitoring demand e registered and also the average PF, during th   | every 15 minutes, calculate the maximum demand edemand interval.   |
|    | Ans :   |  |
|    | Maximum demand registered   | = [ 2940 * (5/15) + 2550 * (7/15) + 2777 * (3/15)]<br>= [ 980 + 1190 + 555.4]<br>= 2725.4 kVA  |
|    | PF<br>5 minutes: 2940 KV/A  | - (2500 / 2940)  |
|    |   | = 0.85   |
|    | 7 minutes 2550 KVA  | = (2500 / 2550)<br>- 0.98  |
|    | 3 minutes 2777 kVA.   | = (2500 / 2777)<br>= 0.90  |
|    | Average PF  | = [ 0.85 *(5/15) + 0.98* (7/15) + 0.9 * (3/15) ]<br>= 0.92   |
| S6 | A process plant has installed 4-cell cooling to<br>at 40 kW at 1450 rpm. As a part of the energy<br>replaced with two speed motors which wou<br>towers are operated at high speed mode for 5<br>a year. | wer, with 45 kW CT fans for each cell and operating<br>y conservation program, the existing fan motors are<br>d operate at 1450 rpm and 740 rpm. The cooling<br>300 hours and at low speed mode for 1800 hours, in |
|    | Estimate the annual energy savings when co speed of 1450 rpm.   | ompared to operation of fans continuously at a fixed   |
|    | Ans :   |  |
|    | Present energy consumption of all 4 fans  | $= (4 \times 40 \times (5300 + 1800))$   |
|    | Energy consumption for fans at 1450 rpm for   | $5300 \text{ hours} = (4 \times 40 \times 5300)$ $= 8 48 000 \text{ kWh}$  |
|    | Energy consumption for fans at 740 rpm for 1  | 800 hours = $[(740/1450)^3 \times 40 \times 4 \times 1800]$<br>= 38281 kWh   |
|    | Annual savings  | = [ 11,36,000 - (8,48,000+38,281) ]<br>= 2,49,719 kWh  |
| S7 | Write short notes on any two of the followi   | ng: (Each 2.5 Marks)   |
|    | <ol> <li>Integrated Part Load Value (IPLV) for</li> <li>Evaporative Cooling</li> </ol>  | chillers   |

|    | 3.             | Heat Pump   |  |                  |
|----|----------------|---|--|------------------|
|    | Ans :          |   |  |                  |
|    | 1.<br>2.<br>3. | Integrated Part Load Value (IPLV) for chillers<br>Evaporative Cooling<br>Heat Pump      | (Page No. 126)<br>(Page No. 136)<br>(Page No. 133) |                  |
| S8 | Write          | short notes on any two of the following:  |  | (Each 2.5 Marks) |
|    | 1.<br>2.<br>3. | Solar Heat Gain Coefficient (SHGC)<br>Visible Light Transmittance (VLT)<br>Cool Roof    |  |                  |
|    | Ans :          |   |  |                  |
|    | 1.<br>2.<br>3. | Solar Heat Gain Coefficient (SHGC),<br>Visible Light Transmittance (VLT),<br>Cool Roof, | (Page No. 272)<br>(Page No. 272)<br>(Page No. 271) |                  |

..... End of Section - II .....

Marks: 6 x 10 = 60

#### Section – III: LONG DESCRIPTIVE QUESTIONS

- Answer all **Six** questions
- (i) (ii) Each question carries Ten marks



| F  | Motor<br>tating in<br>kW   | Operating<br>Load<br>%  | Old Motor<br>Efficiency%   | New Motor<br>efficiency%   | No of mo  | tors                                |
|--|--|---|--|--|---|-------------------------------------|
|  | 7.5  | 75  | 86   | 89   | 12  |                                     |
|  | 11.5   | 85  | 88   | 91   | 7   |                                     |
|  | 15   | 70  | 89   | 92   | 11  |                                     |
| Assumin<br>4000 hou<br>Ans :   | g motor loadir<br>urs operation p  | ng in both cases r<br>ber year.   | emains same, calci   | ulate the ann  | ual energy sa   | avings,                             |
| Motor<br>Rating  | Operating<br>Load  | Actual Old<br>Motor Load  | Actual New<br>Motor Load   | Old<br>Motor   | New<br>Motor  | No o<br>moto                        |
| in KW  | %  | In kW   | In kw  | efficiency   | efficiency  |                                     |
| 7.5  | 75   | 7.5/0.86=8.72<br>=8.72x<br>0.75=6.54  | 7.5/0.89=8.43<br>=8.43x 0.75=<br>6.32  | 86   | 89  | 12                                  |
| 11.5   | 85   | 11.5/0.88=13.07<br>=13.07 x 0.85=<br>11.11  | 11.5/0.91=12.64<br>=12.64 x 0.85=<br>10.74   | 88   | 91  | 7                                   |
| 15   | 70   | 15/0.89=16.85<br>=16.85x 0.7=<br>11.79  | 15/0.92=16.30<br>=16.30 x 0.7<br>11.41   | 89   | 92  | 11                                  |
| 12 numb<br>Annual S<br>7 numbe   | ers, operating<br>avings for 11<br>rs, operating 4   | 4000 hours<br>KW Motors,<br>1000 hours  | :<br>:<br>:  | = [ 4,000 (6.5<br>= 10,560 kWł<br>= [ 4000 (11.1<br>= 10,360 kWł   | 4-6.32) x 12 ַ<br>ו<br>1 -10.74) x 7<br>ו                     | ]                                   |
| Annual S<br>11 numb  | Savings for 15<br>ers operating  | KW Motors,<br>4000 hours  | -  | = [ 4,000 (11.<br><b>= 16,720 kWł</b>  | 79-11.41) x1<br>າ   | 1]                                  |
| Annual S<br>11 numb<br>Total anr   | Savings for 15<br>ers operating<br>nual savings fo   | KW Motors,<br>4000 hours<br>or 30 high efficienc  | ;<br>y motors =  | = [ 4,000 (11.<br>= 16,720 kWł<br>= 37,640 kWł   | 79-11.41) x1<br>າ<br>າ  | 1]                                  |
| Annual S<br>11 numb<br>Total anr<br>A 10 MW<br>11 KV.  | Savings for 15<br>ers operating<br>nual savings fo<br>/ co-generatio   | KW Motors,<br>4000 hours<br>or 30 high efficienc<br>n plant is operatir   | ;y motors =  | = [ 4,000 (11.<br><b>= 16,720 kWf</b><br><b>= 37,640 kWf</b><br>ctor of 85 %.                                  | 79-11.41) x1<br>n<br>Power is ge                              | 1]<br>nerated                       |
| Annual S<br>11 numb<br>Total anr<br>A 10 MW<br>11 KV.<br>> 35 %<br>effici                    | Savings for 15<br>ers operating<br>hual savings fo<br>/ co-generatio<br>of the power<br>ency.                                      | KW Motors,<br>4000 hours<br>or 30 high efficienc<br>n plant is operatir<br>generated, is exp  | ey motors end<br>ng at a daily load fa<br>orted to grid, throug                          | = [ 4,000 (11.<br><b>= 16,720 kWł</b><br><b>= 37,640 kWł</b><br>ctor of 85 %.<br>h a 7.5 MVA                   | 79-11.41) x1<br>n<br>Power is ge<br>Transformer               | 1]<br>nerated<br>with 99            |
| Annual S<br>11 numb<br>Total anr<br>A 10 MW<br>11 KV.<br>> 35 %<br>effici<br>> 32 %<br>trans | Savings for 15<br>ers operating<br>hual savings fo<br>/ co-generatic<br>o of the power<br>ency.<br>o power gener<br>former, with 9 | KW Motors,<br>4000 hours<br>or 30 high efficienc<br>n plant is operatir<br>generated, is exp<br>ated, is supplied to<br>8 % efficiency. | ey motors end<br>ng at a daily load fa<br>orted to grid, throug<br>o mill motors, at 600 | = [ 4,000 (11.<br><b>= 16,720 kWf</b><br><b>= 37,640 kWf</b><br>ctor of 85 %.<br>h a 7.5 MVA<br>0 Volts, throu | 79-11.41) x1<br>n<br>Power is ge<br>Transformer<br>gh a 5 MVA | 1]<br>nerated<br>with 99<br>step do |

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Calculate the following: 1) Daily energy exported to grid at 33 KV. 2) Daily mill motors consumption at 600 V. 3) Daily LT loads and auxiliary consumption at 415 V. 4) Daily transformers losses in kWh and % transformers losses (Each 2.5 Marks) Ans : 1. Daily generation  $= (10,000 \times 0.85 \times 24)$ = 2,04,000 kWh Daily energy generation for export purpose  $= (2,04,000 \times 0.35)$ = 71,400 KWh 7.5 MVA transformer loss  $= [71,400 - (71,400 \times 0.99)]$ =(71,400-70,686)= 714 kWh = (71,400 kWh - 714 kWh) Net energy export to the Grid at 33 KV level =70,686 KWh 2. Daily energy generation for mill motor consumption  $= (2,04,000 \times 0.32)$ = 65,280 kWh 5 MVA Transformer loss  $= [65,280 - (65,280 \times 0.98)]$ = (65,280 - 63,974.4)= 1,306 kWh Net mill Consumption = 63,974 KWh 3. Daily generation for LT loads & Auxiliary consumption  $= (2,04,000 \times 0.33)$ = 67,320 kWh 2MVA Transformer loss = [ 67320 - (67320 x 0.98) ] = 67,320 - 65,974  $= 1,346 \, \text{kWh}$ Net LT loads & Auxiliary Consumption = 65,974 kWh 4. Transformers losses = (714 + 1306 + 1346)= 3,366 kWh day = (3,366 / 2,04,000) x 100 % transformers losses = 1.65 %(Or) To meet the plant LT loads and co-gen auxiliary load, the transformer capacity should be more than 2 MVA.

|  | Shift reference  | Load time in sec   | Un-Load time in sec   |
|--|--|--|---|
|  | (8 hrs/ Shift)   | 60   | 10  |
|  | i  | 45   | 25  |
|  | III  | 25   | 45  |
| Load P<br>Un-loa                       | 'ower =<br>d power = '   | 37 KW<br>11 KW   |   |
| Calcula                                | ate the following:   |  |   |
| 1. Ener<br>2. Shift<br>3. The<br>after | gy loss per day (4 Marks)<br>wise average air requirement<br>plant has proposed to inst<br>r installing the VFD operated | ent in cfm ( 2 Marks)<br>all a VFD for the compressor.<br>d compressor, if the VFD loss is | Calculate the energy sa<br>s 3 % of load power.<br>( 4 Marks) |
| Ans :                                  |  |  | ( i mano)   |
| I <sup>st</sup> shift                  | consumption  | = ((60 / 70) x 37) -   | + (10 / 70) x 11) x 8)  |
|  |  | = (31.71+1.57) x   | 8   |
|  |  | = 266.24 kWh   |   |
| ll <sup>nd</sup> shi                   | ft consumption   | = ((0.64 x 37 + 0.3  | 36 x 11) x 8 )  |
|  |  | = (23.68 + 3.96) x   | 8   |
|  |  | = 221.12 kWh   |   |
| III <sup>rd</sup> shit                 | it consumption   | = ((0.36 x 37 + 0.6  | 64 x 11) x 8)   |
|  |  | = (13.32 +7.04) x  | : 8)  |
|  |  | = 162.88 kWh   |   |
| Daily T                                | otal Energy consumption  | = (266.24 + 221.1  | 2 + 162.88)   |
|  |  | = 650.24 kWh   |   |
|  | nergy loss due to unloading  | = (1.57 +3.96 +7.0   | 04) x 8   |
| Daily E                                |  |  |   |
| Daily E                                |  | = 100.56 kWh   |   |
| Daily E<br>Daily Ic                    | ad cycle Energy consumption  | = <b>100.56 kWh</b><br>on = (650.24 – 100.5  | 6)  |
| Daily E<br>Daily Ic                    | ad cycle Energy consumption  | = 100.56 kWh<br>on = (650.24 – 100.5<br>= 549.68 kWh                                       | 6)  |

|    | Daily Energy loss due to VFD  | = (566.68 - 549.68)         |           |
|----|---|-----------------------------|-----------|
|    |   | = 17 kWh                    |           |
|    | Daily Net Energy savings with VFD compressor = (100.56 – 17)  |                             |           |
|    |   | = 83.56 kWh                 |           |
|    | I <sup>st</sup> shift air requirement   | = (0.86 x 220)              |           |
|    |   | = 189.2 cfm                 |           |
|    | II <sup>nd</sup> shift air requirement  | = (0.64 x 220)              |           |
|    |   | = 140.8 cfm                 |           |
|    | III <sup>rd</sup> shift air requirement   | = (0.36 x 220)              |           |
|    |   | = 79.2 cfm                  |           |
| L5 | (a) What is L/G ratio and how it is useful in operation of a cooling tower ?  |                             | (2 Marke) |
|    | <ul><li>(b) What are the functions of fill media in a cooling tower?</li><li>(c) Calculate the L/G ratio for the cooling tower given the following:</li></ul>                                       |                             | (3 Marks) |
|    |   |                             | (3 Marks) |
|    | Water Flow  | = 4540 m <sup>3</sup> /hour | (4 Marks) |
|    | Approach  | = 4.45 °C                   |           |
|    | Air entering enthalpy at 26.67 °C   | = 24.17 kcal/kg             |           |
|    | Air leaving enthalpy at 37.8 °C   | = 39.67 Kcal/kg             |           |
|    | Hot water temperature   | = 47.77 °C                  |           |
|    | Cold water temperature  | = 31.11°C                   |           |
|    | Ans :   |                             |           |
|    | <b>a)</b> Page 205  |                             |           |
|    | (b) Page 209  |                             |           |
|    | c)  |                             |           |
|    | $\begin{array}{ll} L \ / \ G &= (h_2 \ -h_1) \ / \ (T_1 \ - T_2) \\ L \ (47.77 \ - \ 31.11) &= G \ (39.67 \ - \ 24.17) \\ L \ / \ G \ Ratio &= (39.67 \ - \ 24.17) \ / \ (4 \\ &= 0.93 \end{array}$ | 7.77 - 31.11)               |           |

L6 In an energy audit of a fan, it was observed that the fan was delivering 24,000 Nm<sup>3</sup>/hr of air. a) Suction static pressure was recorded as -15 mm WC and discharge static pressure as 35 mmWC. The power measurement of the motor using power analyzer was recorded as 7 kW. The motor operating efficiency taken from motor performance curve was 90%. What is the static efficiency of the fan? b) Match the Following NPSHR 1. Heat Pump \_ 2. Compressor Static Head 3. Pumping Pressure \_ Static Pressure 4. Fan \_ Compressor 5. Pump Free air delivery test \_ Soln : a) Q = 24.000 Nm<sup>3</sup> / hr. = 6.67 m<sup>3</sup>/sec Static pressure rise = 35 - (-15)= 50 mmWC ηs =? Power input to motor = 7 kW Power input to fan shaft =  $7 \times 0.90 = 6.3 \text{ kW}$ Fan static  $\eta =$ <u>Volume in m<sup>3</sup>/sec x  $\Delta P_{st}$  in mmWc</u> 102 x Power input to shaft  $= (6.67 \times 50) / (102 \times 6.3)$ = 0.519 (or) = 51.9 % Match the Following b) 1. Heat Pump NPSHR (5) \_ 2. Compressor Static Head (3) \_ 3. Pumping Pressure \_ Static Pressure (4) 4. Fan Compressor (1) \_ 5. Pump Free air delivery test (2) \_

----- End of Section - III -----