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Name : \_\_\_\_\_\_(To be written by the candidate)

## 18<sup>th</sup> NATIONAL CERTIFICATION EXAMINATION FOR ENERGY MANAGERS & ENERGY AUDITORS – September, 2017

# PAPER – 2: Energy Efficiency in Thermal Utilities

Date: 23.09.2017 Timings: 14:00-17:00 HRS Duration: 3 HRS Max. Marks: 150

#### General instructions:

- Please check that this question paper contains 8 printed pages
- Please check that this question paper contains 64 questions
- The question paper is divided into three sections
- All questions in all three sections are compulsory
- All parts of a question should be answered at one place

#### Section – I: OBJECTIVE TYPE

Marks: 50 x 1 = 50

- a) Answer all **50** questions
- b) Each question carries **one** mark
- c) Please hatch the appropriate oval in the OMR answer sheet with Black Pen or HB pencil

| 1. | <ul> <li> is required for the simple estimation of flame temperature of the fuel.</li> <li>a) Ultimate analysis</li> <li>b) Proximate analysis</li> <li>c) Size of the coal</li> <li>d) All of the above</li> </ul> |
|----|---|
| 2. | <ul> <li> is required to accommodate expansion of steam lines.</li> <li>a) PRV</li> <li>b) Expansion loop</li> <li>c) Steam trap</li> <li>d) Air vent</li> </ul>  |
| 3. | <ul> <li> is used as heat carrier in thermic fluid heaters</li> <li>a) Steam</li> <li>b) Mineral Oil</li> <li>c) Water</li> <li>d) All of the above</li> </ul>  |

| 4.  | "Heat Loss = Heat gain " is the principle ofa) Boiler                              |                             |                                  |
|-----|--|-----------------------------|----------------------------------|
|     | b) Heat Exchanger  |                             |                                  |
|     | <ul><li>c) Steam traps</li><li>d) All of the above</li></ul>                       |                             |                                  |
|     | ,<br>  | 1.50/                       |                                  |
| 5.  | A boiler trial indicated $2\% O_2$ at boile<br>quantity between these two measurem |                             | $O_2$ at stack. The in-leak air  |
|     | a) 25% b) 40%  | c) 50%                      | d) none of the above             |
| 6.  | A pinch analysis can result in   |                             |                                  |
|     | a) reduction in cooling water<br>c) increase in cooling water                      | b) reduction<br>d) both a & |                                  |
| 7.  | Automatic blowdown controls for bo   | ilers work by s             | ensing                           |
|     | a) TDS <u>b) conductivity</u>  | c) pH                       | d) conductivity and pH           |
| 8.  | Auxiliary power consumption for coa  | al preparation w            | vill be highest in a;            |
|     | a) stoker fired boiler   | b) AFBC bo                  | iler                             |
|     | c) CFBC boiler   | ,                           | ed coal fired boiler             |
| 9.  | Ceramic fibre gives the maximum en   | ergy savings w              | hen used in                      |
|     | a) continuous furnace  | b) batch fu                 | rnace                            |
|     | c) arc furnace   | d) induction                | furnace                          |
| 10. | Degasser in water treatment is used to remove                                      |                             |                                  |
|     | a) Dissolved oxygen and other gas  | b) carbonic                 | acid                             |
|     | b) Sulphuric acid  | d) dissolved                | $CO_2$                           |
| 11. | Dissolved CO2 in boiler feed water<br>ofin boiler tubes                            | when left untro             | eated would result in occurrence |
|     | a)creep <b>b) water side corrosio</b>  | n c)scale                   | d)water hammer                   |
| 12. | Electro static precipitator in FBC boil  | ler is used for _           |                                  |
|     | a) Bottom ash removal  |                             |                                  |
|     | b) Fly ash removal   |                             |                                  |
|     | c) SO <sub>2</sub> removal   |                             |                                  |
|     | d) CO <sub>2</sub> removal   |                             |                                  |
| 13. | Flash steam quantity per kg of conder  | nsate depends u             | ipon                             |

|     | a) condensate pressure onlyb) condensate pressure and flowc) condensate pressure and flash steam pressured) none of the above   |  |  |
|-----|---|--|--|
| 14. | Fluidized bed combustion takes place in the temperature range of  |  |  |
|     | a) above $1000^{\circ}$ C b) below $500^{\circ}$ C c) $600-700^{\circ}$ C d) $800-900^{\circ}$ C  |  |  |
| 15. | <ul> <li>Heat loss through openings in furnaces is directly proportional to</li> <li>a) fourth power of furnace temperature</li> <li>b) square of absolute furnace temperature</li> <li>c) absolute furnace temperature</li> <li>d) fourth power of absolute furnace temperature</li> </ul> |  |  |
| 16. | Heat rate is likely to be the least for   |  |  |
|     | a) back pressure turbine b) condensing turbine  |  |  |
|     | c)extraction condensing turbine d) double extraction turbine  |  |  |
| 17. | In a boiler Theoretical Air to fuel ratio is 15:1. If 10% excess air is supplied, Flue gas to Fuel ratio will be  |  |  |
|     | a) 16:1   |  |  |
|     | b) 17.5:1   |  |  |
|     | c) 16.5:1   |  |  |
|     | d) 17:1   |  |  |
| 18. | In a boiler, air preheater is installed   |  |  |
|     | a) Before the economizer c) after economizer  |  |  |
|     | b) Before superheater d) after ESP  |  |  |
| 19. | In a counter-flow heat exchanger, cold fluid enters at 30°C and leaves at 50°C, whereas the hot fluid enters at 150°C and leaves at 130°C. The LMTD is  |  |  |
|     | a) 100°C b) 280°C c) 0°C d) 20°C  |  |  |
| 20. | In a glass industry waste heat is used for power generation. This type of cogeneration is called  |  |  |
|     | a) topping cycleb) bottoming cyclec) combined cycled) none of the above   |  |  |
| 21. | In a Heat exchanger with a high LMTD results in   |  |  |

|     | a) higher heat transfer areab) lower heat transfer areac) higher u-factord) none of the above  |  |  |
|-----|--|--|--|
| 22. | In a heat exchanger, for the same heat duty, higher the heat transfer coefficient;   |  |  |
|     | <ul> <li>a) higher will be the heat transfer area needed</li> <li>b) higher will be the LMTD</li> <li>c) lower will be the heat transfer area needed</li> <li>d) lower will be the LMTD</li> </ul>   |  |  |
| 23. | In FBC boilers fluidization depends largely on   |  |  |
|     | i) Particle size ii) Air velocityiii) Bed Material iv) Size of Boiler  |  |  |
|     | a) i & iii b) ii & iii c) i & ii d) i,ii,iii,iv  |  |  |
| 24. | In industrial applications the commonly used trap for main steam lines is  |  |  |
|     | a) thermostatic trap<br>b) inverted bucket trap<br>d) open bucket trap   |  |  |
| 25. | Increased Sulphur percentage in furnace oil  |  |  |
|     | a)sets lower flue gas temperature limitb) improves viscosityc) does not add to heat valued) forms soot   |  |  |
| 26. | Insulating material made by blending and melting of alumina and silica is known as   |  |  |
|     | a) ceramic fibre b) high alumina brick c) fire brick d) insulating brick   |  |  |
| 27. | Latent heat of steam at the critical point is  |  |  |
|     | a) infinite b) 540 kcal c) zero d) none of the above   |  |  |
| 28. | <ul> <li>Overall heat transfer co-efficient in Heat exchangers depends on</li> <li>a) Conductivity of the wall separating the two fluids</li> <li>b) Convective coefficients of hot and cold fluids</li> <li>c) Fouling coefficients</li> <li>d) All of the above</li> </ul> |  |  |
| 29. | Select the odd one among the following   |  |  |
|     | a) condenser b) distillation column c) evaporator d) cooling tower   |  |  |
| 30. | Steam mains should be run with a falling slope of in the direction of steam flow for effective line condensate drainage  |  |  |
|     | a) 50 mm in 30 meters b) <b>125 mm in 30 meters</b>  |  |  |
|     | c) 250 mm in 30 meters d) 350 mm in 30 meters  |  |  |
| 31. | Tangential firing is used in which type of boiler:   |  |  |

|     | a) CFBC b) Chain Grate c) Spreader Stoker d) Pulverised Fuel  |  |  |
|-----|---|--|--|
| 32. | The amount of oxygen required to burn 0.5 kg of Sulphur is<br>a) 1<br>b) 16<br>c) 32  |  |  |
|     | d) <b>0.5</b>   |  |  |
| 33. | The concentration of solids in a boiler is controlled by  |  |  |
|     | a) steam venting b) blow down c) air venting d) deaeration  |  |  |
| 34. | The key property of bio mass fuel which influences storage, handling and transportation   |  |  |
|     | a) Calorific Value b) Percentage of Ash   |  |  |
|     | c) Bulk Density d) None of the above  |  |  |
| 35. | <ul> <li>The main contributor for temporary hardness in Boiler water is</li> <li>a) Calcium chloride</li> <li>b) Magnesium Sulphate</li> <li>c) Calcium Bicarbonate</li> <li>d) Calcium nitrate</li> </ul>          |  |  |
| 36. | The turbine heat rate is expressed as   |  |  |
|     | a) kWh/kcal b) kg/kcal c)kcal/kWh_ d) none of the above   |  |  |
| 37. | When 100 kg of fuel with 60% carbon is burnt with theoretical air, the mass of $CO_2$ released will be  |  |  |
|     | a) 319 kg b) 4400 kg c) 4500 kg d) <b>220 kg</b>  |  |  |
| 38. | When solutions of differing concentrations are separated by a semi-permeable membrane, water from less concentrated solution passes through the membrane to dilute the liquid of high concentration. This is called |  |  |
|     | a) reverse osmosis b) ion exchange c) softening d) osmosis  |  |  |
| 39. | When the boiler bed temperature exceeds beyond 950°C, the result is:  |  |  |
|     | a) Low steam temperature b) clinker formation   |  |  |
|     | c) Melting of lime stones d) Ash carry over   |  |  |
| 40. | Which among the following is most viscous fuel?   |  |  |
|     | a) furnace oil b) HSD c) kerosene d) Light Diesel oil   |  |  |
| 41. | Which of the following contributes to spluttering of flame at burner tip during   |  |  |

|     | combustion of fuel oil?  |  |  |
|-----|--|--|--|
|     | <ul> <li>a) ash content</li> <li>b) water content</li> <li>c) sulphur content</li> <li>d) humidity of air</li> </ul>   |  |  |
| 42. | Which of the following heat recovery equipment works on a vapour compression cycle?  |  |  |
|     | a) thermo-compressor b) heat wheel<br>c) heat pump d) heat pipe  |  |  |
| 43. | <ul> <li>Which of the following increases, when steam is passed through PRV?</li> <li>a) Specific volume</li> <li>b) Enthalpy of steam</li> <li>c) Sensible heat</li> <li>d) Saturation temperature</li> </ul> |  |  |
| 44. | Which of the following is an example of a basic refractory   |  |  |
|     | a) Alumino-silicate b) chrome  |  |  |
|     | b) Magnesite d)pure alumina  |  |  |
| 45. | Which of the following is not measured in the ultimate analysis of a fuel ?  |  |  |
|     | a) oxygen b) fixed carbon c) sulphur d) nitrogen   |  |  |
| 46. | Which of the following is not true with respect to improper sizing of coal   |  |  |
|     | <ul><li>a) results in poor combustion</li><li>b) lowers excess air resulting in lesser stack loss</li></ul>  |  |  |
|     | <ul><li>c) increases un-burnt in ash</li><li>d) lowers thermal efficiency</li></ul>  |  |  |
| 47. | Which of the following is true of plate heat exchangersa) close approachb) expandable areac) Counter currentd) All of the above  |  |  |
| 48. | <ul> <li>Which of the following releases large amount of heat per kg during combustion?</li> <li>a) Hydrogen</li> <li>b) Carbon</li> <li>c) Sulphur</li> <li>d) Nitrogen</li> </ul>                            |  |  |
| 49. | Which of the following waste heat recovery systems is of thermal storage type?   |  |  |
|     | a) ceramic recuperator<br>c) regenerative burner<br>b) metallic recuperator<br>d) waste heat boiler  |  |  |
| 50. | Which property of the refractory determines the deformation under stress?  |  |  |
|     | <ul><li>a) Creep</li><li>b) Refractoriness Under Load (RUL)</li></ul>  |  |  |

|  | c) Porosity |  |
|--|-------------|--|
|--|-------------|--|

d) Pyrometric Cone Equivalent (PCE)

----- End of Section - I ------

#### SHORT DESCRIPTIVE QUESTIONS Section - II: Marks: 8 x 5 = 40

- (i) Answer all eight questions(ii) Each question carries five marks

| S-1 | Two identical biomass fired boilers of capacity 10 TPH are operated in a chemical industry. They each have a full load efficiency of 80%. The part load efficiencies at 70% and 40% load are 70% and 68% respectively. For meeting 14 TPH requirement of steam, would you prefer to run both the boilers at 7 TPH capacity or one at full load capacity and other at 40% capacity. Estimate the % savings in the preferred case. |
|-----|--|
| Ans | Fuel energy required when both the boilers are run at 7 TPH load   |
|     | Governing equation to be used :<br>(Fuel reqd) = [(Qty stm) * (Enth steam – Enth feedwater)] / [( GCV Fuel) * (Effy boiler)]   |
|     | (Fuel reqd) = [( $Qty \ stm$ ) * ( $\Delta h$ ) / (Effy boiler)]   |
|     | Where : $\Delta h = is$ same in both cases = [Enth steam – Enth feed-water) / (GCV Fuel)]  |
|     | <i>Fuel required</i> = $(2*7*\Delta h) / (0.70) = 20 \Delta h$   |
|     | 1 mark   |
|     | <u>Fuel energy required when one boiler is running at full load and the other at part load of 40%</u>  |
|     | $\frac{4070}{Fuel required} = \left[ (10^*\Delta h) / (0.8) \right] + \left[ (4^*\Delta h) / (0.68) \right] = 18.38 \Delta h$  |
|     |  |
|     | • The case where one boiler is running at full load and the other at part load of 40% is preferred   |
|     | 1 mark   |
|     | • % savings = $[(20 \Delta h) - (18.38 \Delta h)] * 100 / (20 \Delta h)$<br>= 8.1%   |
|     | 1 mark   |
| S-2 | What happens to steam properties such as saturation temperature, enthalpy of saturated water, latent heat of steam, enthalpy of steam and specific volume of steam, if the steam pressure is increased?  |
|     | a) Saturation Temperature increases  |
| Ans | b) Enthalpy of saturated water Increases.  |
|     |  |
|     | c) Latent heat of steam decreases  |
|     | d) Enthalpy of steam increases   |
|     | e) Specific Volume decreases   |
| 1   |  |

| S-3 | To meet a process plant's heat and power requirements, high pressure steam at 65 MT/h<br>passes through a back pressure steam turbine, for power generation and the exhaus<br>steam is sent for thermal process requirements in the plant. With the following operating<br>data, calculate the heat to power ratio in kW/kW, if the turbine and generator efficiencies<br>are 90% and 92% respectively.  |  |  |
|-----|--|--|--|
|     | Steam Inlet conditions Steam outlet conditions   |  |  |
|     | Pressure= 50 barPressure= 10 barTemperature= 530°CTemperature= 280°CEnthalpy of steam= 3515 kJ/KgEnthalpy= 3020 kJ/KgEnthalpy of water= 782 kJ/kg  |  |  |
| Ans | - Power generated = $65 * 1000 * (3515 - 3020) * 0.92 * 0.90 / 3600$<br>= $7400 \text{ kW}$  |  |  |
|     | - Heat input to process = 65 * 1000 * (3020-782) / 3600 = 40408 kW<br>   |  |  |
|     | - Heat to power ratio = $40408/7400$ = $5.46$ kW/kW  |  |  |
|     | 1 mark   |  |  |
| S-4 | Explain the working of Thermic fluid heating system and why it is preferred to steam heating in some cases?  |  |  |
| Ans | <ul> <li>Thermic Fluid Heaters:</li> <li>At high temperatures, steam requires a corresponding high operating pressure and establishing high temperatures with steam can be very cumbersome and expensive in some cases.</li> <li>In thermic fluid heaters, a special type of oil-synthetic / mineral -is used as heat carrier. This fluid can be heated up to 300°C at atmospheric pressure. In comparison steam would require a pressure of 85 bars to obtain this temperature.</li> </ul>  |  |  |
|     | Advantages:  |  |  |
|     | <ul> <li>High temperature operation at atmospheric pressure</li> <li>Optional temperature level set points</li> <li>No supply or treatment of hot water and hence no heat loss due to condensate flash steam</li> <li>No risk of corrosion</li> <li>Easy to operate</li> <li>Functioning of Thermic Fluid Heaters</li> <li>Heat is transferred to the fluid through radiation. The hot thermic fluid is circulated to various process equipments such as dryers, heaters, deodouriser etc. where it gives up the heat. The return oil at a temperature 10 to 20 °C less comes back to the thermic fluid heater to get heated up</li> </ul> |  |  |

| r   |   |  |  |
|-----|---|--|--|
|     | <ul> <li>The thermic fluid heater operat<br/>the upper limit is reached the b<br/>fire mode. In the case of solid for<br/>reaching the upper limit. When</li> </ul>   | out by a thermic fluid circulation pump.<br>es between two temperature ranges. Once<br>purner is switched OFF or goes into the low<br>uel fired system the ID fan switches OFF on<br>the temperature reaches the lower limit due<br>the burners come ON again and in case of<br>again. |  |
|     | <sup>0</sup> C), the leaving exhaust gas<br>temperature. Hence, the hea<br>component of fuel losses. This of<br>suitable application.   | operate at a high temperature (250 – 300<br>s temperatures are more than the fluid<br>t loss through the flue gas is a major<br>offers potential for heat recovery if there is a<br>ms of Lakh kilo Calories per hour or Million   |  |
|     | kilo Calories per hour.   |  |  |
|     | Pg no 56 of Book 2 for explanation  | 2.5 marks  |  |
| S-5 | In a car manufacture company, Propane is used as fuel in heaters for preheating paints. Calculate the Air to Fuel ratio for complete combustion of $C_3H_8$ (Propane), if 20% excess air is supplied to the heater. |  |  |
| Ans | C <sub>3</sub> H <sub>8</sub> + 5 O <sub>2</sub> > 3 CO <sub>2</sub> + 4 H <sub>2</sub> O   |  |  |
|     | 1 mole of propane requires 5 moles of Oxygen.   |  |  |
|     | Molecular weight of Propane is 44 Kg per mole.  |  |  |
|     | 44 Kg of Propane requires 160 Kg of Oxygen1 mark  |  |  |
|     | Theoretical air required for combustion   | = 160 / 0.23 = 695.6 Kg/hr   |  |
|     | Excess air supplied is 20 %.  | 1.5 marks  |  |
|     | Actual air supplied for combustion is   | = 695.6 * 1.20   |  |
|     |   | = 834.72 Kg/hr of air  |  |
|     | Air to Fuel ratio   | = 834.72 / 44  |  |
|     |   | = 18.97 or <mark>1</mark> 9  |  |
|     |   | 1.5 marks  |  |
| S-6 | a) Explain why de-superheating is done af   | ter pressure reduction in PRVs?  |  |
|     | b) Why is correction factor required for est  | imation of LMTD?   |  |

| Ans | <ul> <li>a) A reduction in steam pressure through a pressure reducing valve (PRV) is an isenthalpic process. Saturated steam when reduced to a lower pressure results in super heated steam. Since process requires only saturated steam, de-superheating is often required, to compensate for superheat gained in PRV application due to isenthalpic expansion.</li> <li>2.5 marks</li> <li>b) In multi pass shell and tube heat exchangers, the flow pattern is a mixture of co-current and counter current flow, as the two streams flow through the exchanger in the same direction on same passes and in the opposite on others. For these reasons, the mean temperature differences is not equal to the logarithmic mean. However it is convenient to retain the LMTD by introducing a correction factor, F which is appropriately termed as the LMTD correction factor.</li> </ul> |  |  |
|-----|---|--|--|
|     |   |  |  |
|     | 2.5 marks   |  |  |
| S-7 | The efficiency of a boiler on GCV basis is 83%. The fuel contains 1.0 % moisture and 12 % hydrogen. The GCV of fuel is 10,500 Kcal/kg. What is the boiler efficiency on the basis of net calorific value?   |  |  |
| Ans | %age of Hydrogen in fuel %age of moisture in fuel<br>NCV = GCV – [9 x++   |  |  |
|     | 100 100   |  |  |
|     | NCV = $10500 - [9 \times \frac{12}{100} + \frac{1.0}{100}] \times 584$  |  |  |
|     | = 10500 - [9 x 0.12 + 0.01] x 584   |  |  |
|     | = 10500 - 636.56  |  |  |
|     | = 9863.44 = 9863 kcal / kg  |  |  |
|     | Boiler efficiency on NCV = $\begin{array}{c} 83\\\\ 9863 \end{array}$ x 10500   |  |  |
|     | = 88.36%  |  |  |
|     |   |  |  |
| S 8 | A reheating furnace is operating with deteriorated wall insulation. The existing average outer surface temperature of the furnace (of area = $100 \text{ m}^2$ ) with surrounding ambient air temperature of $40^{\circ}$ C, is recorded to be $120^{\circ}$ C. After revamping the refractory, the furnace outer surface temperature reduces to $50^{\circ}$ C. If the fuel oil (GCV = $11,000 \text{ kcal/kg}$ ) cost is Rs. 25,000 per tonne, and efficiency of the furnace is 32%, estimate annual savings for 330 working days per year.   |  |  |

| Rate of heat loss from furnace surface (existing)<br>S = [10+(Ts – Ta) / 20] x ( Ts- Ta)   |
|--|
| Heat loss = S x A  |
| = $100m^2 x \left[10 + \left(\frac{120 - 40}{20}\right)\right]$ (120-40) kcals/hr /m <sup>2</sup> = 112.0 x 10 <sup>3</sup> kcal/hr                                    |
| 1 mark   |
| Rate of heat loss from furnace surface after revamping insulation refractory   |
| = 100 [ 10 + $\frac{50-40}{20}$ ] (50-40) = 10.5 x 10 <sup>3</sup> kcal/hr   |
| 1 mark   |
| Energy savings_kcal/hr = 112-10.5_= 101.5x10 <sup>3</sup> kcal/hr<br>Annual energy savings_= (112-10.5) x 10 <sup>3</sup> x 330 x 24 = 8.039 x 10 <sup>8</sup> kcal/yr |
|  |
| Annual fuel oil savings = $\frac{8.039x10^8}{0.32x11000}$ = 2.29 x 10 <sup>5</sup> kg of fuel  |
| 1 mark   |
| Annual Cost savings = $\frac{2.29 \times 10^5 \times 25000}{1000}$ = Rs.5.73 x 10 <sup>6</sup>   |
| 1 mark   |
|  |

----- End of Section - II -----

### Section - III: LONG DESCRIPTIVE QUESTIONS Marks: 6 x 10 = 60

- (i) Answer all SIX questions
- (ii) Each question carries <u>Ten</u> marks

| _   | Write short notes on following refractory properties and their significance.   |  |  |  |  |
|-----|--|--|--|--|--|
| L-1 | a) Porosity b) Bulk density c) Pyrometric cone equivalent d) Thermal conductivity  |  |  |  |  |
| Ans | Porosity   |  |  |  |  |
|     | Low porosity is desirable as it would prevent easy penetration of refractory and also larger<br>number of small pores are preferred over small number of large pores |  |  |  |  |
|     |  |  |  |  |  |
|     | Bulk density   |  |  |  |  |
|     | Increase in bulk density increases its volume stability, heat capacity and resistance to slag  |  |  |  |  |
|     | penetration  |  |  |  |  |
|     |  |  |  |  |  |
|     | Pyrometric Cone Equivalent (PCE)   |  |  |  |  |
|     | temperature at which refractory will deform under its own weight is its softening  |  |  |  |  |
|     | temperature indicated by PCE.  |  |  |  |  |
|     |  |  |  |  |  |
|     | Thermal conductivity   |  |  |  |  |
|     | It is the heat loss per unit area per unit insulation thickness per unit temperature difference  |  |  |  |  |
|     | W-m2/m°C or W-m/°C. Thermal conductivity of materials increases with temperature.  |  |  |  |  |
|     | So thermal conductivity is always specified at the mean temperature (mean of hot and cold face   |  |  |  |  |

|  | temperatures) of the insulation material |  |  |  |                                  |                                |                        |        |  |
|--|--|--|--|--|----------------------------------|--------------------------------|------------------------|--------|--|
|  | <b>Refer Book 2, Page no 156 – 157</b>   |  |  |  |                                  |                                |                        |        |  |
| L-2  | LDO<br>mediu<br>Speci                    | (Light Diesel<br>um. Steam e<br>fic heat of LD | ning unit, a coun<br>Oil) flowing at 6<br>nters the heat e<br>O is 830 kg/m <sup>3</sup> &<br>n at 8 kg/cm <sup>2</sup> is g | 0 m <sup>3</sup> /hr at 50°C<br>exchanger throug<br>a 0.7 kcal/kg°C re | using Ste<br>h a pipe            | am at 8 kg/cm<br>of 6" diamete | ² <sub>g</sub> as a he | eating |  |
|  |  | Pressure,<br>(kg/cm <sup>2</sup> g)            | Temperature,<br>(°C)   | Specific<br>volume<br>(m³/kg)  | (kcal/kg)                        |                                | Steam                  |        |  |
|  |  | 8.0  | 170  | 0.22   | 170                              | 490                            | 660                    |        |  |
| <ul> <li>a. Calculate the mass flow rate of Steam, if the maximum perror the pipeline is 30 m/sec.</li> <li>b. Temperature of the Fuel oil, after preheating in the heat excertains</li> </ul> |  |  |  |  |                                  |                                | city in                |        |  |
|  | Area of the pipe                         |  |  | =  | = 6 inch                         |                                |                        |        |  |
|  |  |  |  | =  | = 6 * 2.54                       |                                |                        |        |  |
|  |  |  |  | =  | = 15.24 cm                       |                                |                        |        |  |
|  |  |  |  | =  | = 3.14 * D <sup>2</sup> / 4      |                                |                        |        |  |
|  |  |  |  | =  | = 3.14* (15.24) <sup>2</sup> / 4 |                                |                        |        |  |
|  |  |  |  | =  | $= 182.3 \text{ cm}^2$           |                                |                        |        |  |
|  |  |  |  | =  | = 0.0182 m <sup>2</sup>          |                                |                        |        |  |
|  |  |  |  | =  | = Area * Velocity                |                                |                        |        |  |
|  |  | Velocity permissible                           |  |  | = 30 m/sec                       |                                |                        |        |  |
|  |  | Volumetric                                     | flow rate of ste   | am =   | = 0.0182 * 30                    |                                |                        |        |  |
|  |  |  |  |  | = 0.546 m <sup>3</sup> /s * 3600 |                                |                        |        |  |
|  |  |  |  | =  | = 1965.6 m³/hr                   |                                |                        |        |  |

|     | Specific volume of steam   | = 0.22 m³/kg                                  |  |  |  |
|-----|--|---|--|--|--|
|     | Mass flow rate of steam  | = 1965.6 / 0.22                               |  |  |  |
|     |  | = 8934.5 kg/hr                                |  |  |  |
|     | a. Mass flow rate of steam   | = 8.93 TPH                                    |  |  |  |
|     |  | 1 mark  |  |  |  |
|     | Temperature of the Fuel oil  |   |  |  |  |
|     | Heat transfer rate of Steam  | = m * H                                       |  |  |  |
|     |  | = 8934.5 * 490                                |  |  |  |
|     |  | = 4377905 kcal/hr                             |  |  |  |
|     | Heat transfer rate of Steam  | = heat transfer rate of LDO                   |  |  |  |
|     | Heat transfer rate of LDO  | = 4377905 kcal/hr                             |  |  |  |
|     | Heat transfer rate of LDO  | = m * Cp * (T <sub>1</sub> – T <sub>2</sub> ) |  |  |  |
|     |  | = 60 * 830 * 0.7 * (T – 50)                   |  |  |  |
|     |  | = 4377905 (60 * 830 * 0.7)                    |  |  |  |
|     | Delta Temperature  | = 125.59°C                                    |  |  |  |
|     | Outlet Temperature of LDO  | = <b>125.59 + 50</b>                          |  |  |  |
|     |  | = 175.59 °C                                   |  |  |  |
|     | b. Outlet temperature of LDO   | = 175.6°C                                     |  |  |  |
|     |  | 2 marks                                       |  |  |  |
| L3  | Write short notes on any two of the following  |   |  |  |  |
|     | a. Wet preservation method for boilers   |   |  |  |  |
|     | b. Reverse osmosis   |   |  |  |  |
|     | c. Reciprocating engine co-generation system   |   |  |  |  |
| ANS | a) Wet preservation method for boilers: In the wet method the boiler is filled to the normal level with water at a pH of 10.5 to 11. Hydrazine to the extent of 200 ppm is to be dosed with the water. The unit is to be steamed in service to ensure uniform concentration of boiler water throughout the unit and to eliminate dissolved oxygen from water. Sodium sulphite (Na <sub>2</sub> SO <sub>3</sub> ), which acts as a de-oxygenerator, can also be used as an alternative to hydrazine and the sulphite concentration has to be maintained at 300-400 ppm. |   |  |  |  |
|     | Analysis of boiler water should be carried out frequently. If the hydrazine concentration in water happens to drop below 50 ppm, the water in the drum should be lowered to the normal   |   |  |  |  |

|     | operating level and an appropriate quantity of chemicals show<br>the concentration of hydrazine or sodium sulphite. The boiler<br>chemicals to uniform concentration.  |   |
|-----|--|---|
|     | b) <b>Reverse osmosis:</b> When solutions of differing concentrate permeable membrane, water from less concentrated solution p dilute the liquid of high concentration, which is called ost concentration is pressurized, the process is reversed and the v concentration flows to the weaker solution. This is known as r   | basses through the membrane to<br>mosis. If the solution of high<br>water from the solution of high   |
|     | c) <b>Reciprocating engine co-generation system:</b> Also (I. C.) engines, these cogeneration systems have high por comparison with other prime movers. There are two sources gas at high temperature and engine jacket cooling water system recovery can be quite efficient for smaller systems, these s smaller energy consuming facilities, particularly those having than thermal energy and where the quality of heat required steam or hot water.  | known as internal combustion<br>wer generation efficiencies in<br>s of heat for recovery: exhaust<br>em at low temperature. As heat<br>ystems are more popular with<br>g a greater need for electricity<br>is not high, e.g. low pressure |
| L4  | <ul> <li>A fluidized bed boiler generates 24TPH at 22 kg/cm<sup>2</sup>(g), our the back pressure turbine and exhausts from it at 5kg/cm<sup>2</sup>(requirement in the plant. The balance steam from the boiler supply 10 kg/cm<sup>2</sup>(g) steam at saturated condition (dry satu DM water at 105°C is used for de-superheating in PRDS. Given data: <ul> <li>a) Mechanical Efficiency of steam turbine</li> <li>b) Losses in gear transmission</li> <li>c) Efficiency of alternator</li> <li>d) The total heat of steam at turbine inlet condition at 2</li> </ul> </li> </ul> | g) to meet the process steam<br>is passed through a PRDS to<br>rated) to the another process.<br>= 94 %<br>= 5%<br>= 95 %<br>22 kg/cm <sup>2</sup> (g) = 708 kcal/kg<br>5 kg/cm <sup>2</sup> (g) = 658 kcal/kg                            |
|     | <ul> <li>f) The total heat of the steam at PRDS exit at 10kg/cm<sup>2</sup>(g)</li> <li>Calculate</li> <li>1. Power generation from back pressure turbine</li> </ul>   | = 670 kcal/kg   |
| A   | <ul> <li>2. Steam flow rate going to process at the exit of PRDS</li> <li><u>1: Power generation from back pressure turbine:</u></li> </ul>  |   |
| Ans | Enthalpy drop across the turbine per kg of inlet stean   | n = (h1-h2)   |
|     |  | = (708-658)= 50 kcal/kg   |
|     | Total steam flow rate through turbine<br>Total enthalpy drop across the turbine  | 1 mark<br>= 18,000 kg/hr<br>=18,000*50<br>= 900000 kcal/hr  |
|     | Mechanical Efficiency of steam turbine<br>Efficiency of alternator<br>% losses in gear transmission<br>Over all efficiency of the turbo alternator   | 1 mark<br>= 94%<br>= 95 %<br>= 5%<br>= 0.94 x 0.95 x 0.95   |
|     |  | = 0.848 = 84.8%   |

|     |   |                   |              |                        | 2 marks       |
|-----|---|-------------------|--------------|------------------------|---------------|
|     | Energy output of turbing  |                   |              | = 900000 x 0           |               |
|     | Energy output of turbine  |                   |              |                        | .040          |
|     |   |                   |              | = 763200               | 1 1           |
|     |   |                   |              |                        | 1 mark        |
|     | Power output of the alternator  |                   |              | = 763200 / 860         | = 887.4 kW    |
|     |   |                   |              |                        | 1 mark        |
|     | 2: Steam Flow rate going to proc  | cess at the ex    | cit of PR    | DS:                    |               |
|     | Flow rate of DM water   | = m               |              |                        |               |
|     | Heat content of steam at exit of  | PRDS = Heat       | t supplie    | d by water and ste     | am to PRDS    |
|     |   | x 670 = (600)     |              | -                      |               |
|     |   |                   |              | r = 403.54  kg/hr      |               |
|     |   | m = 403.          | 34 Kg/ 11    |                        | 2 manles      |
|     |   | 000               | 0 . 400      |                        |               |
|     | Steam flow at outlet of PRDS  | = 600             |              | 54 = 6403.54 kg /      |               |
|     |   |                   |              |                        | l mark        |
| L-5 | In a chlor-alkali plant, 100 TPD cau  | istic solution at | t 30% cor    | centration is dried to | o 55%         |
| - • | concentration in a single effect eva  |                   |              |                        |               |
|     | removal is 1.0 kg/kg. It is proposed  | to be replaced    | d by a trip  | le effect evaporator   | at an         |
|     | investment cost of Rs. 5 crore, for   | •                 | •            | •                      |               |
|     |   |                   |              | -                      |               |
|     | kg/kg. Steam for the evaporator is  | generated from    | h an oll fir | ed boller at an evap   | oration ratio |
|     | of 14.3.  |                   |              |                        |               |
|     | Calculate annual fuel savings in TF   | D.                |              |                        |               |
| Ans | % salt concentration at inlet   | = 30%             | 6            |                        |               |
|     | % salt concentration at outlet  | = 55%             |              |                        |               |
|     | Input quantity of caustic solution to   |                   |              |                        |               |
|     |   |                   |              |                        | 1 1           |
|     | Amount of bone dry salt at drier inlet  |                   |              |                        |               |
|     | Amount of water at drier inlet  |                   |              | = 70 TPD               |               |
|     | Flow rate of salt solution at drier ou  | tlet = 30 /       | 0.55         | = 54.5 TPD             | 1 mark        |
|     | Amount of water at drier outlet   | = 54.5            | 5 - 30       | = 24.5 TPD             | 1 mark        |
|     | Amount of water removed   |                   |              | = 45.5 TPD             |               |
|     |   | -                 | -4.5         |                        |               |
|     | Ratio of steam / moisture for single  |                   |              |                        | 1 mark        |
|     | Amount of steam required for singl  | e effect = 45.5   | TPD          |                        |               |
|     | Ratio of steam / moisture for triple  | effect $= 0.54$   | Ļ            |                        |               |
|     | Amount of steam required for triple   | e effect = 45.5   | 5 X 0.54     | = 24.57 TPD            | 1 mark        |
|     | Amount of steam saved by triple eff   |                   |              | = 20.93 TPD            |               |
|     | • •   |                   |              | = 20.93 IPD            | 1 IIIaIK      |
|     | Evaporation ratio   | = 14.3            | -            |                        |               |
|     | Amount of fuel savings  |                   |              | <b>1.464 TPD</b>       |               |
| L-6 | In an engineering industry, an electric   |                   |              |                        |               |
|     | the components. The annealing cycle and corresponding energy consumption as follows.                  |                   |              |                        |               |
|     |   |                   |              |                        |               |
|     | S.No Heat treatment   | Temperature       | Time hrs     | Power drawn in         |               |
|     | cycle   | <sup>~0</sup> C   |              | kW                     |               |
|     | 1 Heat -Up  | 30 - 850          | 4            | 500                    |               |
|     | 2 Holding at  | 850               | 4            | 100                    | ]             |
|     | 3 Cooling   | 850 - 60          | 4            | 20                     | 1             |
|     |   | u                 |              |                        | <b>_</b>      |
|     | The electrical energy drawn in each sub-cycle is uniform and plant operates 50 batches per month.     |                   |              |                        |               |
|     | The cost of electricity is Rs.8/kWh.  |                   |              |                        |               |
|     | The management has decided to replace the electric furnace with FO oil fired furnace with efficiency  |                   |              |                        |               |
| L   | The management has decided to replace the electric furnace with 1.0 on fired furnace with effectively |                   |              |                        |               |

# Paper 2 – Set B with Solutions

|     | of 48%. The cost of F.O is Rs.30/kg. Calculate cost savings and payback period of converting from electric to oil fired furnace. Investment for FO fired furnace is Rs.25 lakhs. The GCV of F.O is 10,000 kcal/kg |                       |   |  |  |
|-----|---|-----------------------|---|--|--|
| Ans | Energy consumption per treatment batch :  |                       |   |  |  |
|     | – Heat up time  | = 500 x 4             | = 2000kWh;1 mark                              |  |  |
|     | <ul> <li>Holding time</li> </ul>  | = 100  x 4            |   |  |  |
|     | <b>~</b>  | = 100 x 4<br>= 20 x 4 |   |  |  |
|     | - Cooling time  | $= 20 \times 4$       |   |  |  |
|     | - Total energy consumption per batch  |                       | $= 2480 \text{ kWh} \dots 1 \text{ mark}$     |  |  |
|     | <ul> <li>Monthly energy consumption by</li> </ul>   |                       |   |  |  |
|     | electric annealing furnace including losses   |                       | = 2480  x  50                                 |  |  |
|     |   |                       | = 1,24,000 kWh / month                        |  |  |
|     |   |                       | 1 mark  |  |  |
|     | – Actual consumption by the components  |                       |   |  |  |
|     | at electrical furnace efficiency of 82%   |                       | = (124000  x  0.82)                           |  |  |
|     |   |                       | = 1,01,680 kWh / month                        |  |  |
|     |   |                       | 1 mark  |  |  |
|     | – Eqvt FO required to be supplied to the oil  |                       |   |  |  |
|     | fired furnace at an efficiency of 50%   |                       | $= 101680 \times 860 / (10000 \times 0.48)$   |  |  |
|     |   |                       | = 18217.67  kg / mth                          |  |  |
|     |   |                       | 1.5 marks                                     |  |  |
|     | <ul> <li>Annual Cost of savings</li> </ul>  |                       | = [(124000  x  8) - (18217.67  x  30)]  x  12 |  |  |
|     | <b>6</b>  |                       | = Rs.53,45,639 / yr                           |  |  |
|     |   |                       | 1.5 marks                                     |  |  |
|     | – Payback period  |                       | = 2500000 / 5345639 = 5.61 months             |  |  |
|     | r uj ouok portoù  |                       | 1 mark  |  |  |
| ]   |   | of Section –          |   |  |  |

<sup>.....</sup> End of Section – III .....