16th NATIONAL CERTIFICATION EXAMINATION FOR ENERGY MANAGERS & ENERGY AUDITORS – September, 2015

	PAPER – 3: Energy Efficienc	y in Electrical Utilitie	S
Date: 20.09.2015	Timings: 0930-1230 HRS	Duration: 3 HRS	Max. Marks: 150

General instructions:

- Please check that this question paper contains 8 printed pages
- Please check that this question paper contains **64** questions
- The question paper is divided into three sections
- All questions in all three sections are compulsory
- All parts of a question should be answered at one place

Section – I: OBJECTIVE TYPE

Marks: 50 x 1 = 50

- i) Answer all **50** questions
- ii) Each question carries **one** mark
- iii) Please hatch the appropriate oval in the OMR answer sheet with Black Pen or HB pencil

1.	Which of the following is not a part of v	apour compress	ion refrigeration cycle:							
	a) compressor b) e	evaporator	c) condenser	d) <u>absorber</u>						
2.	Which of the following can be attributed	d to commercial	loss in electrical distribution sy	stem						
	a) lengthy low voltage lines <u>c) faulty consumer service meters</u>	b) low load si d) undersize c	de power factor conductors							
3.	Which loss in a distribution transformer is dominating; if the transformer is loaded at 68% of its rated capacity									
	a) core loss b) <u>copper loss</u> c)	hysteresis loss	d) magnetic field loss							
4.	When evaporator temperature is reduc	ed								
	a) refrigeration capacity increases c) specific power consumption remains		refrigeration capacity decrease compressor will stop	<u>s</u>						
5.	What is the function of drift eliminators	in cooling tower	S							
		 a) maximize water and air contact b) capture water droplets escaping with air stream c) enables entry of air to the cooling tower d) eliminates uneven distribution of water into the cooling 								
6.	Trivector meter measures three vectors	s representing								
	a) active, reactive and maximum dema c) active, harmonics and maximum de		active, power factor and appare active, reactive and apparent p							

7.	. Time of the Day metering (TOD) is a way to							
	a) reduce the peak demand of the distribution company b) increase the revenue of the distribution							
	company c) increase the peak demand d) increase the maximum demand in a industry							
8.	The unit of specific humidity of air is:							
	a) grams moisture/kg of dry airb) moisture percentage in airc) grams moisture/kg of aird) percentage							
9.	The purpose of inter-cooling in a multistage compressor is to							
	a) remove the moisture in the airb) reduce the work of compressionc) separate moisture and oil vapourd) none of the above							
10.	The percentage reduction in distribution loses when tail end power factor raised from 0.85 to 0.95 is							
	a) 10.1% b) <u>19.9%</u> c)71% d)84%							
11.	The nomenclature T2,T5,T8 and T12 for fluorescent lamps are categorized based on							
	a) diameter of the tubeb) length of the tubec) both diameter and length of the tubed) power consumption							
12.	The inexpensive way to improving energy efficiency of a motor which operates consistently at below 40% of rated capacity is by							
	a) operating in star modeb) replacing with correct sized motorc) operating in delta moded) none							
13.	The indicator of cooling tower performance is best assessed by							
	a) wet bulb temperature b) dry bulb temperature c) range d) approach							
14.	The illuminance of a lamp at one meter distance is 10 Lm/m ² . What will be the corresponding value at 0.7 meter distance							
	a)14.28 b) 20.41 c) 10 d) none of these							
15.	The fan system resistance is predominately due to							
	a) more bends used in the ductb) more equipments in the systemc) volume of air handledd) density of air							
16.	The cooling tower size is with the entering WBT when heat load, range and approach are constant.							
	a) directly proportional b) inversely proportional c) constant d) none of above							
17.	The components of two part tariff structure for HT & EHT category consumers are							
	 a) one part for capacity(or demand) drawn and second part for actual energy drawn b) one part for actual Power Factor and second part for actual energy drawn c) one part for capacity(or demand) drawn and second part for actual reactive energy drawn d) one part for actual apparent operation of actual energy drawn 							
10	d) one part for actual apparent energy drawn and second part for actual reactive energy drawn The adsorption material used in an adsorption air dryer for compressed air is							
18.								

	a) calcium chloride b) magnesium chloride c) <u>activated alumina</u> d) potassium chloride								
19.	The actual measured load of 1000 k VA transformer is 400 k VA. Find out the total transformer loss corresponding to this load if no load loss is 1500 Watts and full load Copper Loss is 12,000 Watts								
	a) 1920 watts b) 1500 watts <u>c) 3420 watt</u> d) 13500 watts								
20.	The percentage imbalance when line-line voltages are 415 V, 418 V and 408 V is								
	a) 4.047% b) 0.22% c) 4.44% d) none of the above								
21.	a) 1.047%b) 0.32%c) 1.44%d) none of the aboveStar – delta starter of an induction motor								
21.									
	 a) reduces voltage by inserting resistance in rotor circuit b) reduces voltage by inserting resistance in stator circuit c) reduces voltage through a transformer <u>d) reduces the supply voltage due to change in connection configuration</u> 								
22.	. Slip power recovery system is applicable in case of								
	a) squirrel cage induction motor. b) wound rotor motor c) synchronous motor d) DC shunt motor								
23.	Rotating magnetic field is produced in a								
	a) single- phase induction motor b) three- phase induction motor								
	c) DC series motor d) all of the above								
24.	Power factor is highest in case of								
	a) sodium vapour lamps b) mercury vapour lamps c) fluorescent lamps d) incandescent lamps								
25.	Power factor Improvement will result in								
	a) reduction in active powerb) reduction in active currentc) reduction in reactive powerd) all the above								
26.	Motor efficiency will be improved by								
	a) r <u>educing the slip</u> b) increasing the slip								
	c) reducing the diameter of the motor d) decreasing the length of the motor								
27.	Lower power factor of a DG set demands								
	a) lower excitation currentsb) no change in excitation currentsc) higher excitation currentsc) none of the above								
28.	L / G ratio in cooling tower is the ratio of								
	a) length and girth b) length and gradient of temperature								
	<u>c) water mass flow rate and air mass flow rate</u> d) water volume flow rate and air volume flow rate								
29.	Installing larger diameter pipe in pumping system results in								
	a) increase in static headb) decrease in static headc) increase in frictional headd) decrease in frictional head								
30.	Installation of Variable frequency drives (VFD) allows the motor to be operated with								
	a) constant current b) lower start-up current c) higher voltage d)none of the								

	above	
31.	. In a no load test of a poly-phase induction motor, the me	asured power by the wattmeter consists of:
	a) core lossb) coppec) core loss, windage & friction lossd) stator	r loss copper loss, iron loss, windage & friction loss
32.	 In a large compressed air system, about 70% to 80% of the 	moisture in the compressed air is removed at
	a) air dryer b) <u>after cooler</u> c) air receiv	ver d) inter cooler
33.	B. Illuminance of a surface is expressed in	
	a) radians <u>b) lux</u> c) lumens	d) LPD
34.	If two identical pumps operate in series, then the combin	ed shutoff head is
	a) it does not affect head b) more than double	<u>c) doubled</u> d) less than
35.	5. If the speed of a reciprocating pump is reduced by 50 %.	the head
	a) is reduced by 50%b) is reduced bc) remains samed) none of the a	
36.	If the observed temperature in air receiver is higher that for free air delivery will be:	n ambient air temperature the correction factor
	a) less than one b) greater than one c) equal to	one d)equal to zero
37.	7. If the COP of a vapour compression system is 3.5 and the motor efficiency, the cooling effect of vapour compression	
	<u>a) 34 kW</u> b) 37.8 kW c) 0.36 kW	d) none of the above
38.	B. If EER of One Ton Split AC is 3.5, what is its power ratin	g?
	<u>a) 1.0 k W</u> b) 1.5 kW c) 0.8 kW	d) None of the above
39.	. Humidification involves	
	 a) reducing wet bulb temperature and specific humidity b) reducing dry bulb temperature and specific humidity c) increasing wet bulb temperature and decreasing specific d) reducing dry bulb temperature and increasing specific 	
40.	. Higher COP can be achieved with	
	 a) lower evaporator temperature and higher condenser t b) higher evaporator temperature and Lower condenser c) higher evaporator temperature and higher condenser d) lower evaporator temperature and Lower condenser t 	temperature temperature
41.	. Friction losses in a pumping system is	
40	c) proportional to square of flow d) inv	versely proportional to cube of flow versely proportional square of flow
42.	Plow control by damper operation in fan system will	

	a) increase energ c) reduce system			b) r<u>educe energy con</u>d) none of the above	sumption		
43.				he following current re = 50 A, fifth harmonic	eadings. Current at 50 current = 35 A		
	a) 58 %	b) 48 %	<u>c) 24%</u>	d) 34 %			
44.		nsity of air at 11400 m and Gas constant:84		sure and 65ºC. (Molec mole K)	cular weight of air:		
	a) 1.2 kg/m ³ b) 1.5 kg/m ³ c) 1.15 kg/m^3 d) none of the above						
45.	A spark ignition e	engine is used for firin	g which type of fuels	:			
	a) high speed die	esel b) li	ght diesel oil	c) <u>natural gas</u>	d) furnace oil		
46.		has four floors each 3000W, the Lighting			ower allowance for the		
	<u>a) 10.75</u>	b) 0.09	c) 43	d) data insuffic	zient		
47.		mes 70 litres per hou at that load, then what			ption of this DG set is		
	a) 212 kVA	b) <u>265 kVA</u>	c) 170 kVA	d) none of th	ne above		
48.		alled a 130 kVAr, 60 kVAr. The reason out	•	•	dicates that it is only		
	a) operating at lo	w load b)	nigh voltage	c) l <u>ow voltage</u>	d) low current		
49.	A 50 hp motor wi 25 kW. The perce		y rating of 90 percer	nt was metered and fo	ound to be operating at		
	a) 75%	b) 50%	<u>c) 60%</u>	d) 25%			
50.		/, 45A, 0.8 PF, 1475 t will be the rated effic		se induction motor op	erating at 420 V, 40 A		
	<u>a) 85.0%</u>	b) 94.5%	c) 89.9%	d) 88.2%			

 End	of	Section –	I	 	• •	 	 	-	

Section – II: SHORT DESCRIPTIVE QUESTIONS

Marks: 8 x 5 = 40

- (i) Answer all <u>Eight</u> questions(ii) Each question carries <u>Five</u> marks

S-1	List five energy saving measures for air conditioning system.

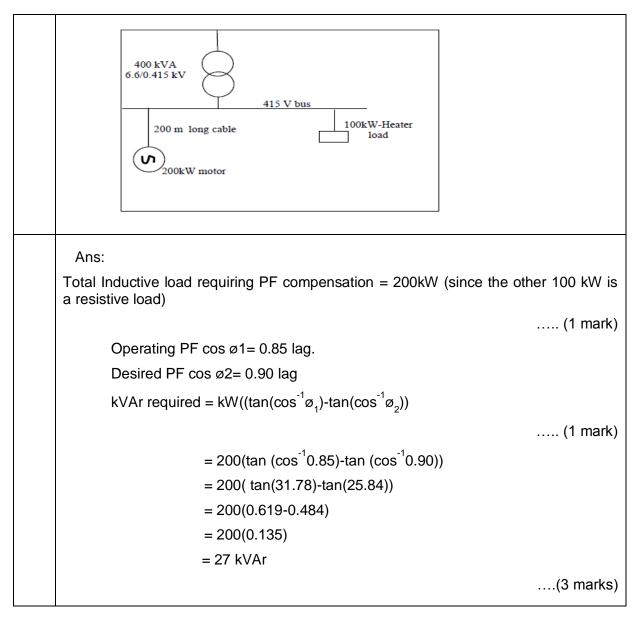
	Insulate all cold lines / vessels using economic insulation thickness to minimize heat gains.
	• Optimize air conditioning volumes by measures such as use of false ceiling and segregation of critical areas for air conditioning by air curtains.
	 Minimize the air conditioning loads by measures such as roof cooling, roof painting, efficient lighting, pre-cooling of fresh air by air- to-air heat exchangers Variable volume air system Optimal thermo-static setting of temperature of air conditioned spaces Sun film application
	 Minimize the process heat loads by measures involving TR reduction and refrigeration temperature level reduction Flow optimization Heat transfer area increase to accept higher temperature coolant Avoid wastages by heat gains Avoid wastages by loss of chilled water Avoid wastages by ideal flows. Frequent cleaning and descaling of all heat exchangers
	At refrigeration and AC plant area
	 Minimize part load operations by matching loads and plant capacity on line; adopt variable speed drives for varying load. Ensure regular maintenance of all AC plant components as per manufacturers guide lines. Ensure adequate quantity of chilled water flows, cooling water flows Avoid by pass flow by closing valves of ideal equipment Adopt VAR system where economics permit as non CFC solutions Make efforts to continuously optimize condenser and evaporator parameters for minimizing specific energy consumption and maximizing capacity
	(5 marks for relevant points as above)
S-2	The total system resistance of a piping loop is 50 meters and the static head is 15 meters at designed water flow. Calculate the system resistance offered at 75%, 50% and 25% of water flow

	Solution:									
	Total System Resistance of piping loop: 50m Static Head :15 m So, Dynamic Head at designed water flow: 35m (2 mark)									
	SI.No.	Flow%	Dynamic Head (m) = 35 x (%flow) ²	Static Head (m)	Total Resistance (m)					
	1	75.0%	19.68	15	34.68					
	2	50.0%	8.75	15	23.75					
	3	25.0%	2.19	15	17.19					
				-	(3 marks-(each 1	mark))				
S-3	In a DG set, the generator is rated at 1000 kVA, 415V, 1390 A, 0.8 PF, 1500 RPM. The full load specific energy consumption of this DG set as measured by the energy auditor is 4.0 kWh per liter of fuel and air drawn by the DG set is 14 kg/kg of fuel. The energy auditor has recommended a waste heat recovery (WHR) system. Also the auditor indicated that the waste heat recovery potential is 2.6x10 ⁵ kCal/hr at the existing engine exhaust gas temperature of 583°C.									
		The specif	ust temperature to chi ic gravity of fuel oil is							

	1	Rated kVA of Diesel Generator (given)	1000	
	2	Rated kW @ 0.8 pf	800	0.5 mark
	3	Specific fuel consumption (kWh/lts) (given)	4	
	4	Specific gravity of fuel oil (given)	0.86	
	5	Oil consumption at full load in kg/hr ((2*4)/3)	172	1 mark
	6	Air supplied per kg of fuel (kg) (given)	14	
	7	Mass of flue gas (14+1)	15	
	8	Mass of flue gas kg per hour (7*5)	2580	1 mark
	9	Waste heat recovery potential kCal/hr (given)	2,60,000	
	10	Delta T across waste heat recovery system (Heat kCal/hr)/(mass of flue gas kg/hr*specific heat, kcal/kg ⁰ C) = (260000/2580x0.25)	403	1.5 mark
	11	Present Flue gas temp. or temp. before waste heat	583	•
		recovery system (given)		
-4	diame	Exit flue gas temp. after waste heat recovery system (583 – delta T) nput power to a fan is 30kW for a 2500 Nm ³ /hr flu ter is 300mm. If the flow to be reduced by 15% by o should be the diameter of fan pulley and power input to	changing th	
-4	The in diame	Exit flue gas temp. after waste heat recovery system (583 – delta T) nput power to a fan is 30kW for a 2500 Nm ³ /hr flu ter is 300mm. If the flow to be reduced by 15% by o should be the diameter of fan pulley and power input to	uid flow. Th	e fan pulle
-4	The in diame what s Solutio	Exit flue gas temp. after waste heat recovery system (583 – delta T) nput power to a fan is 30kW for a 2500 Nm ³ /hr flu ter is 300mm. If the flow to be reduced by 15% by o should be the diameter of fan pulley and power input to on	uid flow. Th changing th fan.	e fan pulle
4	The in diame what s Solution	Exit flue gas temp. after waste heat recovery system (583 – delta T) nput power to a fan is 30kW for a 2500 Nm ³ /hr flu ter is 300mm. If the flow to be reduced by 15% by o should be the diameter of fan pulley and power input to on Input power to fan kW	uid flow. Th changing th fan. 30	e fan pulle
4	The in diame what s Solution	Exit flue gas temp. after waste heat recovery system (583 – delta T) nput power to a fan is 30kW for a 2500 Nm ³ /hr flu ter is 300mm. If the flow to be reduced by 15% by should be the diameter of fan pulley and power input to on Input power to fan kW Fluid flow Nm ³ /hr	uid flow. The changing the fan.	e fan pulle
4	The in diame what s Solution	Exit flue gas temp. after waste heat recovery system (583 – delta T) nput power to a fan is 30kW for a 2500 Nm ³ /hr flu ter is 300mm. If the flow to be reduced by 15% by o should be the diameter of fan pulley and power input to on Input power to fan kW Fluid flow Nm ³ /hr Diameter of Fan pulley (mm)	uid flow. Th changing th fan. 30 2500 300	e fan pulle
-4	The in diame what s Solution	Exit flue gas temp. after waste heat recovery system (583 – delta T) nput power to a fan is 30kW for a 2500 Nm ³ /hr flu ter is 300mm. If the flow to be reduced by 15% by should be the diameter of fan pulley and power input to on Input power to fan kW Fluid flow Nm ³ /hr Diameter of Fan pulley (mm) Governing Equation is N ₁ D ₁ =N ₂ D ₂	uid flow. Th changing th fan. 30 2500 300 Eqn-1	e fan pulle
-4	The in diame what s Solution 1 2 3 4 5	Exit flue gas temp. after waste heat recovery system (583 – delta T) nput power to a fan is 30kW for a 2500 Nm ³ /hr flu ter is 300mm. If the flow to be reduced by 15% by o should be the diameter of fan pulley and power input to on Input power to fan kW Fluid flow Nm ³ /hr Diameter of Fan pulley (mm) Governing Equation is N ₁ D ₁ =N ₂ D ₂ N ₂ = 0.85N ₁	uid flow. The changing the fan. 30 2500 300 Eqn-1 given	e fan pulle e fan pulle
-4	The in diame what s Solution 1 2 3 4 5 6	Exit flue gas temp. after waste heat recovery system (583 – delta T) nput power to a fan is 30kW for a 2500 Nm ³ /hr flutter is 300mm. If the flow to be reduced by 15% by a should be the diameter of fan pulley and power input to on Input power to fan kW Fluid flow Nm ³ /hr Diameter of Fan pulley (mm) Governing Equation is N ₁ D ₁ =N ₂ D ₂ N ₂ = 0.85N ₁ From Eqn-1 D ₂ =(D ₁)*(N ₁ /N ₂); = (300)*(N ₁ /0.85N ₁) (KW ₁ /KW ₂) = (N ₁ ³ /N ₂ ³);	uid flow. Th changing th fan. 30 2500 300 Eqn-1 given 352mm	e fan pulle e fan pulle 1 mark 2 marks
-4	The in diame what s Solution 1 2 3 4 5 6 7	Exit flue gas temp. after waste heat recovery system (583 – delta T) nput power to a fan is 30kW for a 2500 Nm ³ /hr flu ter is 300mm. If the flow to be reduced by 15% by o should be the diameter of fan pulley and power input to on Input power to fan kW Fluid flow Nm ³ /hr Diameter of Fan pulley (mm) Governing Equation is N ₁ D ₁ =N ₂ D ₂ N ₂ = 0.85N ₁ From Eqn-1 D ₂ =(D ₁)*(N ₁ /N ₂); = (300)*(N ₁ /0.85N ₁) (KW ₁ /KW ₂) = (N ₁ ³ /N ₂ ³); Hence, KW ₂ =(N ₂ /N ₁) ^{3*} (KW ₁) =(0.85 N ₁ /N ₁) ^{3*} (30)	uid flow. The changing the fan. 30 2500 300 Eqn-1 given	e fan pulle e fan pulley
-4	The in diame what s Solution 1 2 3 4 5 6 7 So P	Exit flue gas temp. after waste heat recovery system (583 – delta T) nput power to a fan is 30kW for a 2500 Nm ³ /hr flutter is 300mm. If the flow to be reduced by 15% by a should be the diameter of fan pulley and power input to on Input power to fan kW Fluid flow Nm ³ /hr Diameter of Fan pulley (mm) Governing Equation is N ₁ D ₁ =N ₂ D ₂ N ₂ = 0.85N ₁ From Eqn-1 D ₂ =(D ₁)*(N ₁ /N ₂); = (300)*(N ₁ /0.85N ₁) (KW ₁ /KW ₂) = (N ₁ ³ /N ₂ ³);	uid flow. Th changing th fan. 30 2500 300 Eqn-1 given 352mm	e fan pulle e fan pulle 1 mark 2 marks

	4.70									
	uniform	ly distributed over	lluminance produce r a surface area o unit of illumination,	f one square r	neter. It i	s also de	fined as			
						(2.	5 marks)			
		uminous efficacy	is defined as the	ratio of luminou	is flux em	itted by a	lamp to			
	the pow		the lamp. Efficacy							
	(2.5 marks)									
S-6	During an energy audit of a power plant cooling tower, the following observations were made.									
	•	Power plant genei	ration = 7	85 MW						
		Circulation rate		07000 m ³ /hr						
		Cooling tower rang	-	0.5°C						
		•	n COC value = 3							
		ower plant desig		.0 0						
	a) ⁻ b) 5 The pla	Specific water con ant is pursuing an	nsumption per hou sumption in m ³ /M up-gradation treati e potential water sa	<i>N</i> generation. ment plan to inc						
	Ans									
	S.No.	Item Ref.	Calculation		value	units				
	1	Evaporation loss	0.00085*Circulati on rate in m ³ /hr * (CT range in deg	0.00085 * 107000 * (10.5)*1.8	1719	m³/hr	0.5 mark			
			C)*1.8							
	2	Blow-down loss	Evaporation loss/(COC-1)	1719/ (3.8-1)	614	m³/hr	0.5 mark			
	3	Total as run hourly consumption	S.No 1 + S.No 2	(1719+614)	2333	m³/hr	0.5 mark			
	4	Specific water consumption	S.No. 3/785	(2333/785)	2.97	m³/MW	0.5 mark			
	5	Blow down at improved COC of 7.0	Evaporation loss/(COC-1)	1719/(7-1)	286.5	m³/hr	0.5 mark			
	6	Total water consumption at improved COC	S.No 1 + S.No 5	(1719+286.5)	2005.5	m³/hr	0.5 mark			
	7	Specific water consumption at	S.No 6/785	(2005.5/785)	2.56	m³/MW	0.5 mark			

							- I		
		improved COC							
	8	Total water	S.No 3 - S.No 6	(2333-	327.5	m³/hr	0.5 mark		
		saving per hour		2005.5)		0/2			
	9	Water	S.No 8/785	(327.5/785)	0.417	m³/MW	1 mark		
		saving/MW							
		generation							
0.7		with a supplicy for							
S-7	(a) (b)	condenser temper COP _{Carnot} does no	s achieved with hig rature. ot take into accour	nt the type of c	ompresso		ower		
	(C)	How is the COP n	ormally used in th	e industry give	en?				
	Ans:								
 a) The theoretical Coefficient of Performance (Carnot), COP_{Carnot} - a measure of refrigeration efficiency of an ideal refrigeration system- de two key system temperatures, namely, evaporator temperature condenser temperature Tc with 						stem- dep	ends on		
	COP being given as: COP _{Carnot} = Te / (Tc - Te) (2 marks)								
	eva a r	aporator temperation atio of temperation	o indicates that h ure and lower con ures, and hence	denser tempe	rature. Bu	t COP _{Carn}	ot is only		
	compressor (2 marks)								
	c) Hence the COP normally used in the industry is given by								
	COP = [Cooling effect (kW)/Power input to compressor (kW)]								
	where the cooling effect is the difference in enthalpy across the evaporator and expressed as kW								
							(1 mort)		
							(1 mark)		



..... End of Section - II

REGULAR

Section – III: LONG DESCRIPTIVE QUESTIONS

Marks: $6 \times 10 = 60$

- (i) Answer all <u>Six</u> questions
 (ii) Each question carries <u>Ten</u> marks

	SI. No.	Parameter	Centrifug Chiller		AM
	1	Chilled water flow (m ³ /h)	192	1	83
	2	Condenser water flow (m ³ /h)	245	3	60
	3	Chiller inlet water temperature (°C)	13	14	4.5
	4	Condenser water inlet temperature (°C)	28	3	32
	5	Chiller outlet water temperature (°C)	7.8	ç).2
	6	Condenser water outlet temperature (°C)	36.2	4	0.7
	7	Chilled water pump consumption (kW)	32		31
	8	Condenser water pump consumption (kW)	38	Ę	52
	9	Cooling tower fan consumption (kW)	9	2	22
Solu	ii) iii) iv)	Refrigeration load delivered (TR) for both sys Condenser Heat load (TR) for both systems? Compare auxiliary power consumption for bo If electricity cost is Rs.4.0/kWh and steam operating cost for both systems.	, th systems, g		pare the
	ii) iii) iv) ition:	Condenser Heat load (TR) for both systems? Compare auxiliary power consumption for bo If electricity cost is Rs.4.0/kWh and steam	, th systems, g		pare the
	ii) iii) iv) Ition: a) Con	Condenser Heat load (TR) for both systems? Compare auxiliary power consumption for bo If electricity cost is Rs.4.0/kWh and steam operating cost for both systems.	, th systems, g		pare the
; SI	ii) iii) iv) ution: a) Con	Condenser Heat load (TR) for both systems? Compare auxiliary power consumption for bo If electricity cost is Rs.4.0/kWh and steam operating cost for both systems.	th systems, g cost is Rs.0 Centrifugal).45/kg comp	2 marks
SI No	ii) iii) iv) ution: a) Con	Condenser Heat load (TR) for both systems? Compare auxiliary power consumption for bo If electricity cost is Rs.4.0/kWh and steam operating cost for both systems. npression Chiller vs. VAM Parameter frigeration load delivered (TR) Mass of Chilled water flow x Specific heat x Delta T of Chilled water SI. No.1 m ³ /hr * 1000kg/m ³ *1 kcal/kg ⁰ C *	th systems, g cost is Rs.0 Centrifugal Chiller).45/kg comp	

	l					1		
		The auxiliary power consumption in cas because heat rejection in VAM condense				2 marks		
		centrifugal chiller with approximate similar			nighter than	ZIIIdIKS		
	4	Total Energy Consumption:		284 kW (Auxiliary Power of 79kW and Chiller onsumptio n of 205	Auxiliary Power of 105 kW and Steam consumpti on of 1620 kg/hr	2 marks		
	5	Operating Energy Cost per Hour of Operat	ion		Kg/TI			
				Rs. 1136/-	Rs 1149/-			
				(284 * 4 = Rs. 1136/-)	(105 * 4 = Rs. 420/- plus 1620 * 0.45 = Rs. 729/-)	2 marks		
L-2	 a) Calculate the ventilation rate for an engine room of 20m length, 10.5m width height; if the recommended Air Changes per Hour (ACH) is 20. b) Air at 25,200 m³/hr and at 1.2 kg/m³ density is flowing into an air handling u inspection room. The enthalpy difference between the inlet and outlet air is 2.38 k 							
	the n	notor draws 22 kW with an efficiency of 90%, m. (1 cal = 4.183)						
	Solut	ion:						
	a)	Ventilation Rate:						
		Room Length (m)		20				
		Room Height (m)		15				
		Room Width (m)		10.5				
		Air Changes per Hr (ACH)		20				
		Ventilation rate (m ³ /Hr) = Length (m) * Height (m) * Width (m) * ACH		63000				
	b)				(5 marks)			
	b)		Q x ρx (25200 x 71,971	x 1.2 x (2.38 kcal/hr	, C			
			71,971 23.8 TR	/3024	(2 marks)			

										• •	
	Power input to the compressor				(1 mark) 22 x 0.9= 19.8 kW						
	kW/TR				(1 mark) 19.8/23.8 = 0.83						
	KVV/IR				19	.8/23.8	= 0.83		(1 ma	ark)	
L-3									ational sure of		
		Operating Pu	imp No		F	low Ra (m³/hr)					
		Pump No 1 8	<u>k</u> 2			545					
		Pump No 2 8				535					
		Pump No 3 8				550					
	 efficiency for pump no. 3 is 91.5%. If the water level in suction of all pumps is 3 below pump central line. Calculate the following: i) Individual pump efficiencies ii) Specific energy consumption (kWh/m³) iii) Which is the best operating pump combination 									meter	
	Solution:										
	Let flow of pump 1,2	& 3 be X, Y ar	nd Z res	specti	vely.						
	From given:										
	X + Y = 545(1										
	Y + Z = 535(2	,									
	X + Z = 550(3	3)									
	Subtracting eqn (2) f	rom eqn (1):									
	X – Z = 10(4)										
	Adding eqn (3) and e	eqn (4):									
	2X = 560 X= 280										
	Putting X value in eq	n (1) and (2):									
	Y = 265 and Z = 270										
	Therefore, individua	I pump flow	rates	are:	280	m³/hr,	265	m³/hr	and	270	m³/hr

	respectively (3 marks)								
	Pump Ref:	1	2	3]				
	A) Flow Rate (M ³ /hr) <i>(calculated)</i>	280	265	270					
	B) Discharge Head (m) =3.4 kg/cm ² (a)	200	200	2.0					
	= 2.4 kg/cm ² (g) =24 m <i>(given)</i>	24	24	24	-				
	C) Suction Head (m) (g) (given)	-3	-3	-3					
	D) Total Head (Discharge Head - Suction Head)* (<i>B</i> - <i>C</i>)	27	27	27	1 mark				
	E) Liquid kW [flow (m ³ /s)*total head (m)*density (1000 kg./m ³) * 9.81 (m/s ²)/1000]	20.60	20.22	19.87	2 marks				
	F) Power Drawn by motor kW (given)	33	31.5	32.5					
	G) Motor eff. % (given)	92.0%	92.0%	91.5%					
	H) Pump input power kW (FxG)	30.36	28.98	29.74	1 mark				
	I) Pump eff. % (E/H)	67.9%	69.8%	66.8%	1 mark				
	J) Specific Energy Consumption (kWh/M ³) (F/A)	0.118	0.119	0.120	1 mark				
	Pump No. 1 & 2 are the best performing operating combination (1 mark)Note: *The total head has been calculated subtracting Discharge Gauge pressure from suction gauge pressure. The candidates can also calculate total head as difference of absolute pressures as follows:Discharge Head= 3.4 kg/cm^2 (a) Suction Head = $1 - 0.3 \text{ kg/cm}^2 = 0.7 \text{ kg/cm}^2$ Total Head Developed = $3.4 - 0.7 = 2.7 \text{ kg/cm}^2 = 27 \text{ m}$								
L-4	 a) In a chemical industry, cooling water of 9000 m³/hr and 6000 m³/hr from two independent heat exchangers with temperature of 41°C and 52°C respectively are fed to one cooling tower after proper mixing at top basin. If measured heat rejection by the cooling tower is 45,000TR, calculate effectiveness and evaporation loss of the cooling tower at 31°C WBT. b) In an air conditioning duct 0.5 m x 0.5 m, the average velocity of air measured by vane anemometer is 28 m/s. The static pressure at suction of the fan is -20 mmWC 								
	and at the discharge is 30 m/S. The static press and at the discharge is 30 mmWC. A three p 415 V with a power factor of 0.9. Find out ef 88% (neglect density correction)	ohase indu	iction mot	or draws	10.8 A at				

	Solutio	on:				
	a)					
		SI. Io.	Particulars	Stream 1	Stream 2]
	1		Flow Rate (m ³ /hr) (given)	9000	6000	
	2		Temp. ^o C (given)	41	52	
	3		Mix. Flow Rate (m ³ /Hr) (Sl.1 +2)	150	000	
	4		Mix. Hot Water Temp. ^o C [(Flow1 * Temp. 1) + (Flow 2 *Temp. 2)]/ (Flow1 + Flow 2)	45.4		1 mark
	5		Heat Rejection (TR) (given)	450	000	
	6 Ra		Range of Cooling Tower ⁰ C: (Heat Rejection TR * 3024) / (Flow M ³ /hr * 1000)	9.0)72	1 mark
	7		WBT ^o C (given)	3	1	_
	8		Cold Water Temp. ⁰ C (Mix. Hot Water Temp. – Range)	36.	328	0.5 mark
	9		Approach ⁰ C (Cold Water Temp. – WBT)	5.3	328	0.5 mark
	10		Effectiveness (Range/ (Range + Approach))	6	3	1 mark
	11		Evaporation Loss (m ³ /hr) = 0.00085*1.8*Mix. Flow m ³ /hr*Range	20	8.2	1 mark
	b)					
		1	Area of the Duct: (0.5*0.5) m ²	0.	25	
		2	Avg. velocity (m/s) (given)	2	8	
		3	Air Flow (m ³ /s) (SI. 1* SI. 2)	7	7	1 mark
		4	Suction static Pr. (mmWC) (given)	-2	20	
		5	Discharge Static Pr. (mmWC) (given) 3	0	
		6	Power drawn by the motor (kW): (1.732 * 415*10.8*0.9/1000)	6.	99	1 mark
		7	Air Power kW: = Flow (m ³ /s)* (Dis. Pr – Suc. Pr.) mmWC /102	3.	43	1 mark
		8	Power to fan Shaft kW (Motor Drawn power * Motor eff. Of 889	6.	15	1 mark
		9	Fan Static Eff. (%) = Air Power*100%/Shaft Input		.76	1 mark
L-5	plant i proces of stea 127 K Kcal/h	maxir ss an am a cal/m ır. If t	process industries has installed 18 MW cog mum condenser load is 7 MW and the extra d also for vapour absorption machine. The nd the steam rate is 5 kg/KW for condense in/TR and the capacity of VAM is 1100 TR. the tower is designed for 6°C range, calculate approach temperature of the CT is 5°C.	action stea condenser er power. Estimate c	m of 57 TI heat load The heat lo cooling tow	PH is used for is 550 Kcal/kg bad of VAM in er heat load in

-	1		
	Ans.	Condenser load = 7 MW	
		Steam rate for condenser = 5 kg/KW	
		Total steam required for condenser power = 7000 X 5 = 35000 Kg/h	r.
			(2 marks)
		Condenser heat load = 35000 x 550 = 19250000 Kcal/hr.	
			(2 marks)
		Heat load of VAM = 1100 x 127 x 60 = 8382000 Kcal/hr.	
			(2 marks)
		Total heat load = 19250000 + 8382000 = 27632000 Kcal/hr.	(,
			(2 marks)
		Range of tower = 6 deg C	(2 marks)
		Cooling water Flow required=27632000/6=4605333 lts or 4605 m ³ .	
			(2 marks)
L-6	a) List	five disadvantages of low Power Factor ?	
	0.88.7 penalt presci improv	industry is losing money as penalty on account maintaining a poor p The power utility has specified a minimum power factor of 0.9 to avoin ty on energy cost is 1% for every 0.01 power factor less than ribed. Also an incentive on energy cost is available @ 1.5% for vement above 0.95. If the monthly energy bill of the industry is Rs 6 is not cost saving potential if power factor is improved to unity from the	d penalty. The the minimum or every 0.01 akhs, calculate
	Answe		
	a) Dis	(Any five -1 mark each) advantages of low power factor are 1.) Large Line Losses (Copper Losses) 2.) Large kVA rating and Size of Electrical Equipments 3.) Greater Conductor Size and Cost 4.) Poor Voltage Regulation and Large Voltage Drop 5.) Low Efficiency 6.) Penalty from Electric Power Supply Company on Low Power fact	
	Prese For 0. Incent Energ Cost r	num PF to be maintained to avoid penalty = 0.9ent penalty= 1.00 % (on energy bill) for every 0.01 P.F. $02 PF$ = 1.00 x 2 = 2.0%tives= 1.5 x 5 = 7.5%tives= 1.5 x 5 = 7.5%ty saving potential= 9.5%reduction potential per month = 6 lakh x 9.5%= Rs.57000al cost Reduction= 57000x12 = Rs.684000	

----- End of Section - III -----

REGULAR